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## 1. GENERAL

The rf tray is a compartmentalized casting that houses and provides shielding for various radio assemblies as shown in Figures 1 and 2.

The rf tray also provides mounting for the receiver pre-selector filter as shown in Figure 2. A detailed description of the rf tray interconnect board as well as uniboard parts information is included in this section. All other assemblies are described in their respective sections of this manual.

## 2. INTERCONNECTIONS

### 2.1 INTERCABLING

The rf tray cabling shown in Figure 3, routes various signals and control functions throughout the station. Refer to the simplified functional block diagram in the Description section of this manual for specific connection details.

### 2.2 INTERCONNECT BOARD

The interconnect board, mounted beneath the rf tray casting (see Figure 3), provides connections between cir-

cuit boards and assemblies located in the rf tray. Feed-through plates mounted in the rf tray as shown in Figure 4, provide isolation between the interconnect board, circuit boards, and assemblies contained in the rf tray casting. Additional shielding and isolation are provided by covers over critical circuit areas and compartments, by metal braid between compartments, and by the rf tray cover. A connection chart and interconnect circuit board detail are included at the end of this section.

## 3. UNIBOARD

The uniboard contains portions of the station receiver and transmitter circuits. These portions include:

- Receive Synthesizer Circuitry
- Receiver I-F Amplifier and Detector
- Transmit Synthesizer Circuitry
- Power Control Circuitry
- Synthesizer Reference Oscillator

Refer to Figure 7 for circuit location and interconnect details. All of these circuits are described in detail in related sections of the manual. Complete parts list information is included in this section.

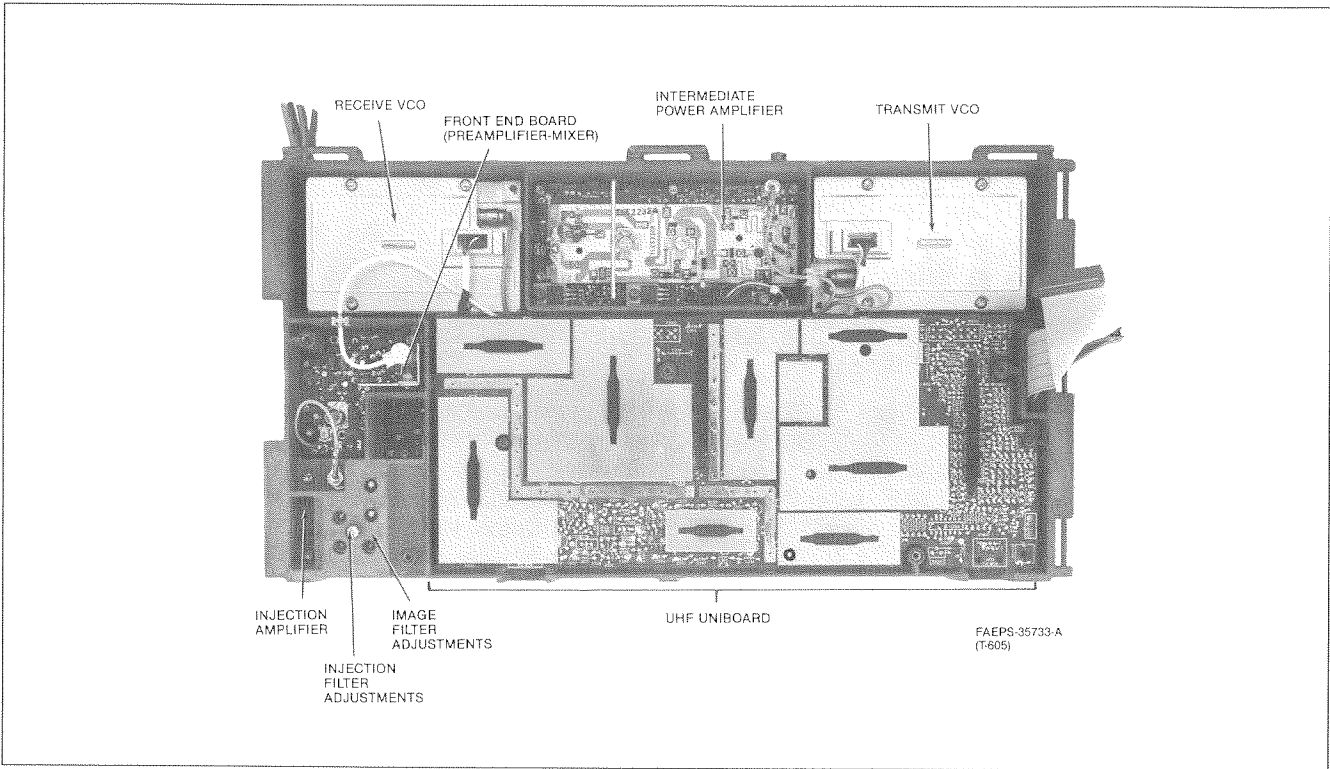


Figure 1. RF Tray Assembly Location Detail (Top View)

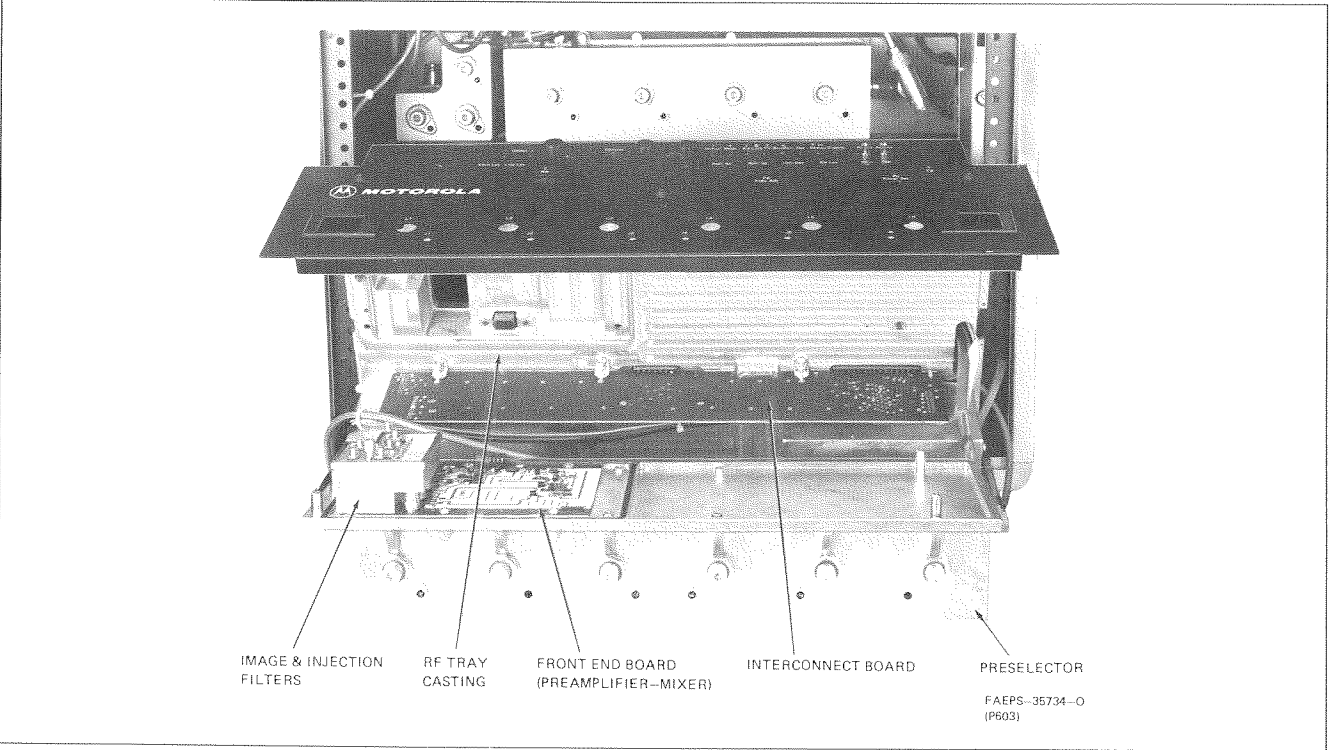


Figure 2. RF Tray Assembly Location Detail (Bottom View)

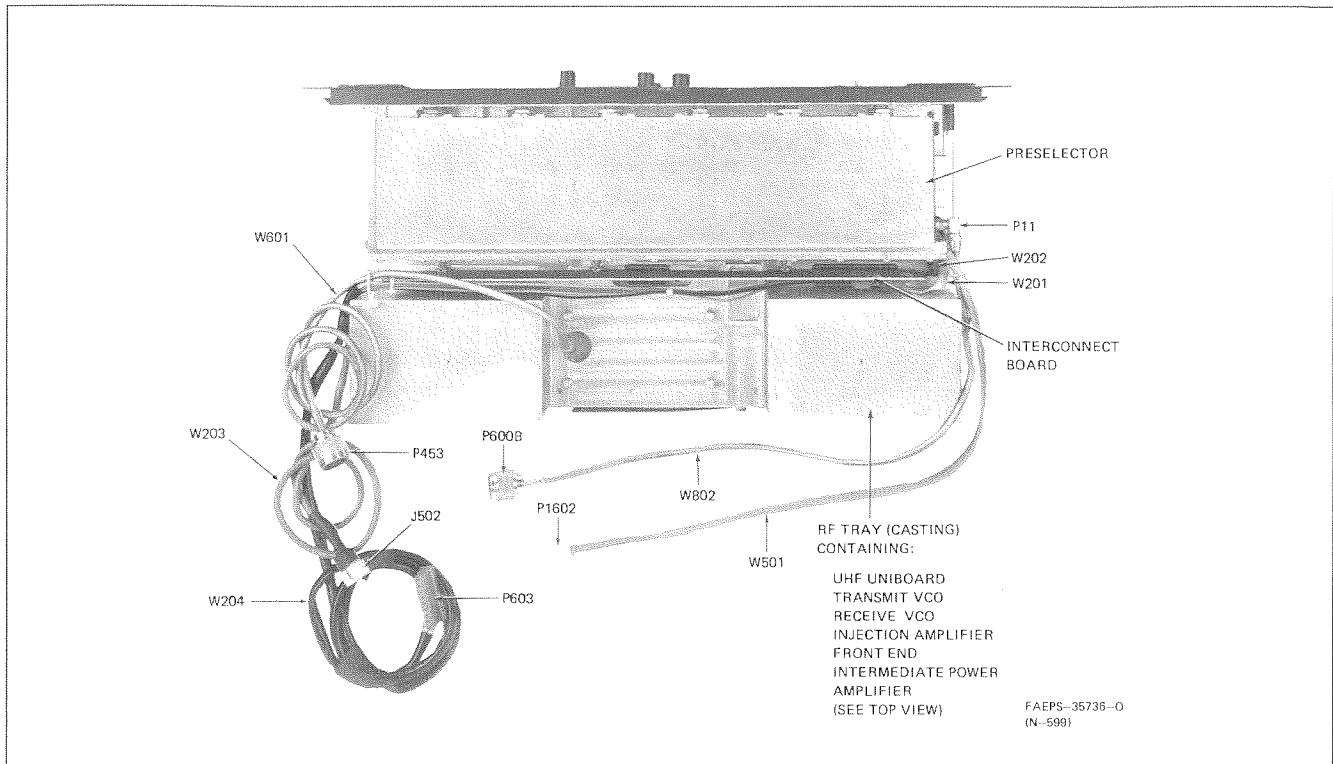


Figure 3. RF Tray Bottom View

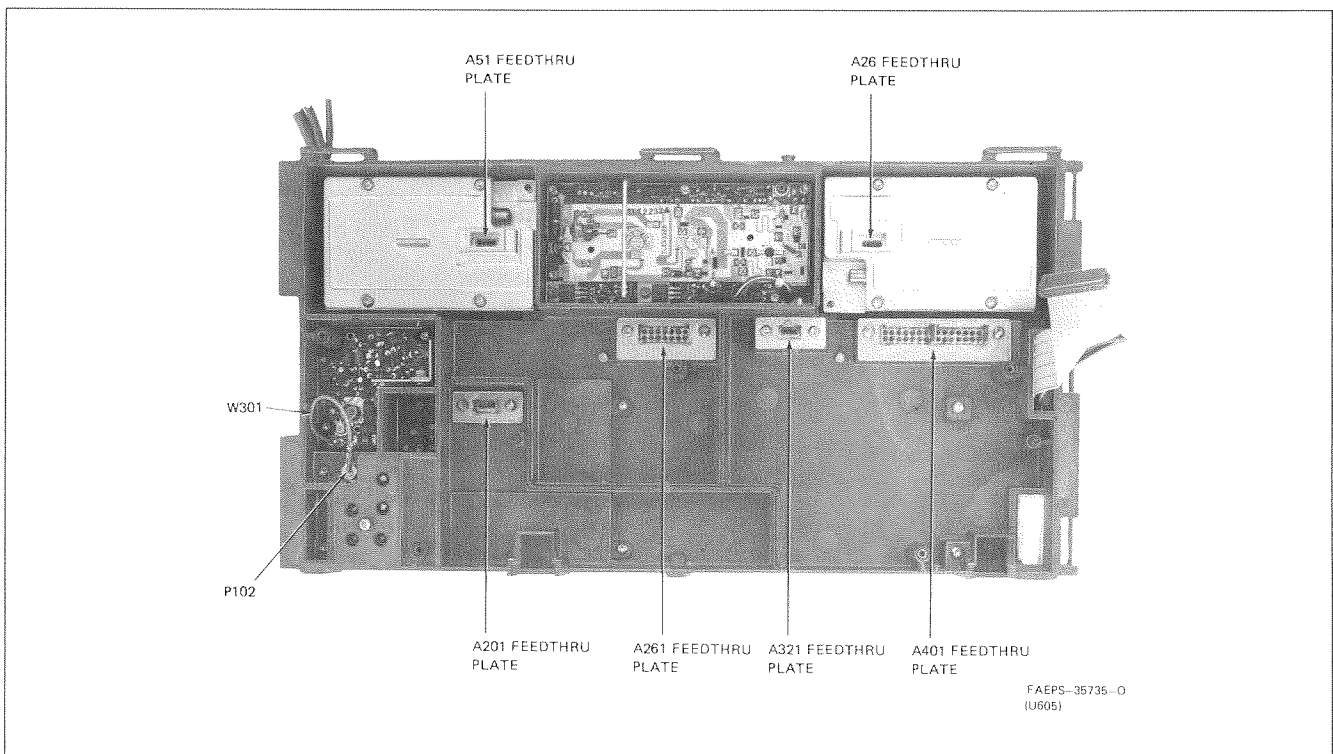


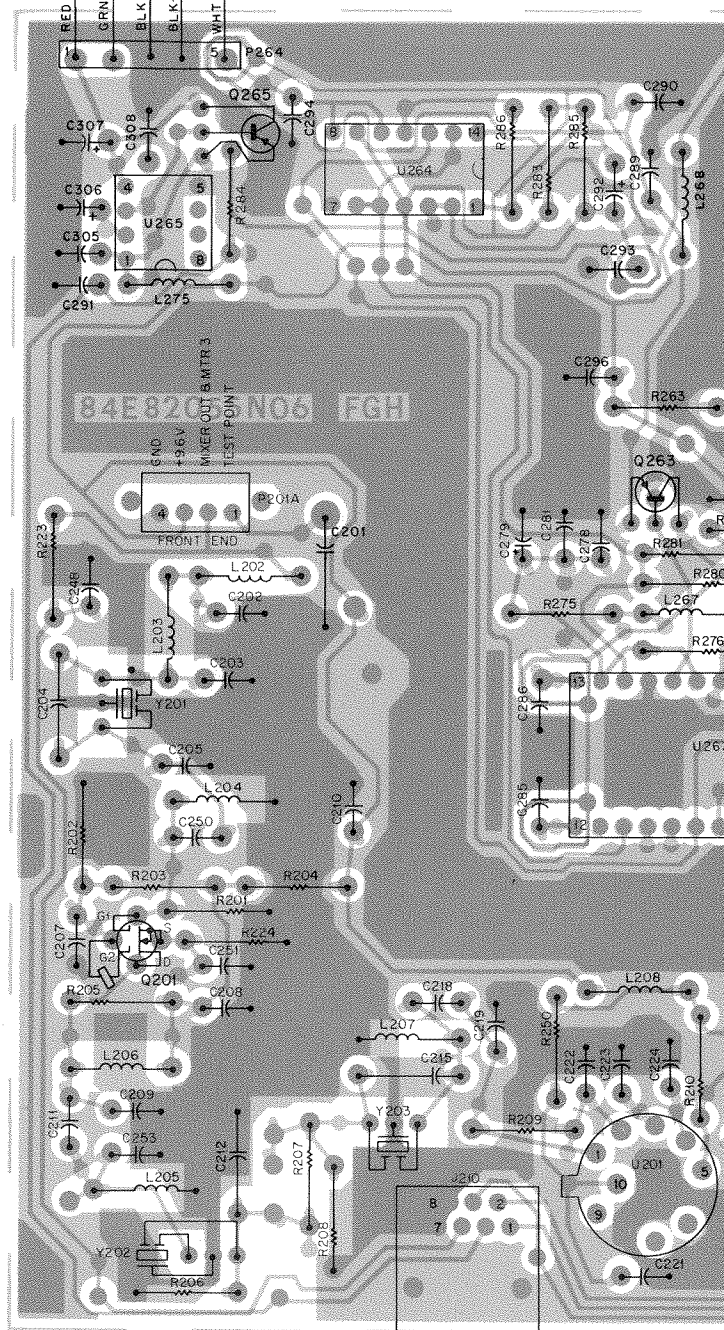
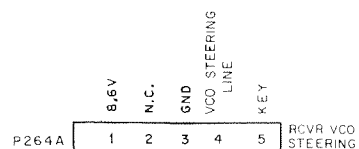
Figure 4. RF Tray Assembly Feedthru Detail (Uniboard Removed)



# UNIBOARD

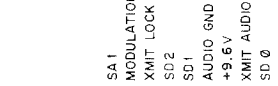
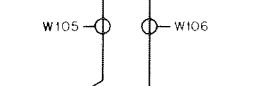
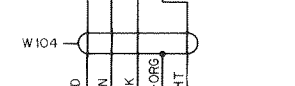
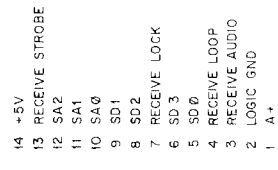
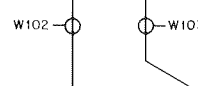
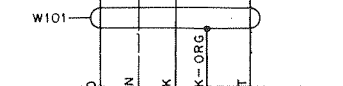
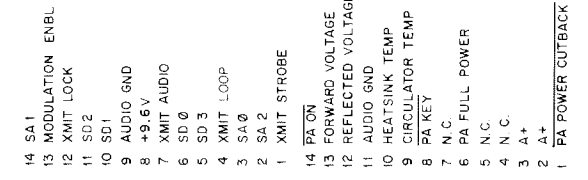
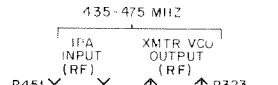
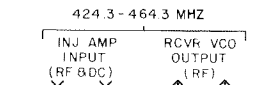
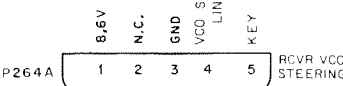
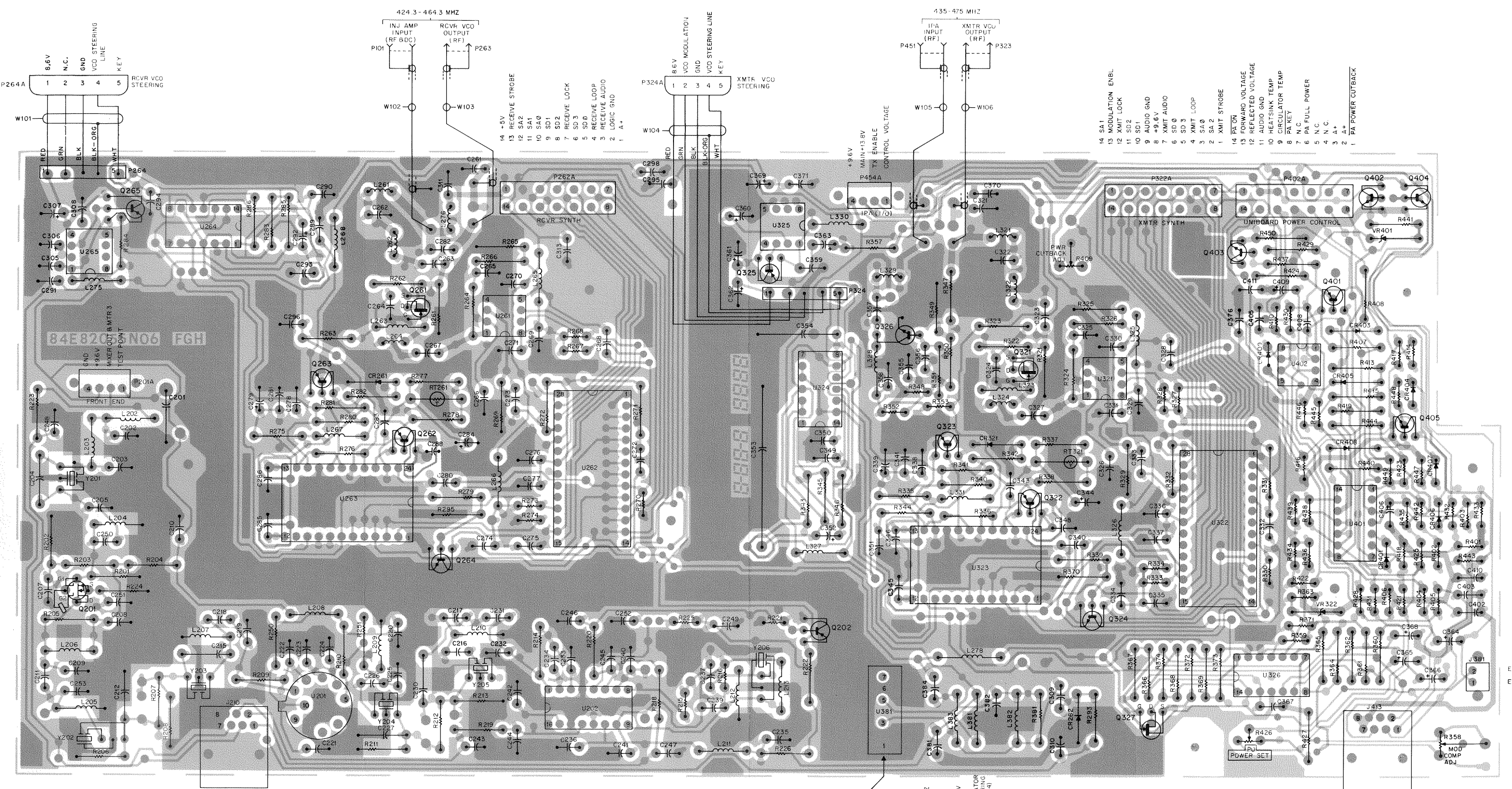
## COMPONENT SIDE DETAIL

### MODEL TRN9880A



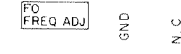
- RX  
METERING
- 6-8 GND
  - 5 RCVR SYNTH
  - 4 STEERING LINE
  - 3 REFERENCE
  - 2 OSCILLATOR
  - 1 MIXER
  - INJECTION
  - 1-F LEVEL
  - QUADRATURE
  - DETECTOR

REFER TO APPROPRIATE  
MANUAL SECTION FOR  
SCHEMATIC DIAGRAMS



- 6-8 GND
- 5 RCVR SYNTH
- 4 STEERING LINE
- 3 REFERENCE
- 2 OSCILLATOR
- 1 MIXER INJECTION
- 1 I-F LEVEL
- 1 QUADRATURE DETECTOR

SHOWN FROM SOLDER SIDE

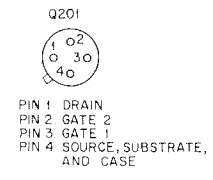
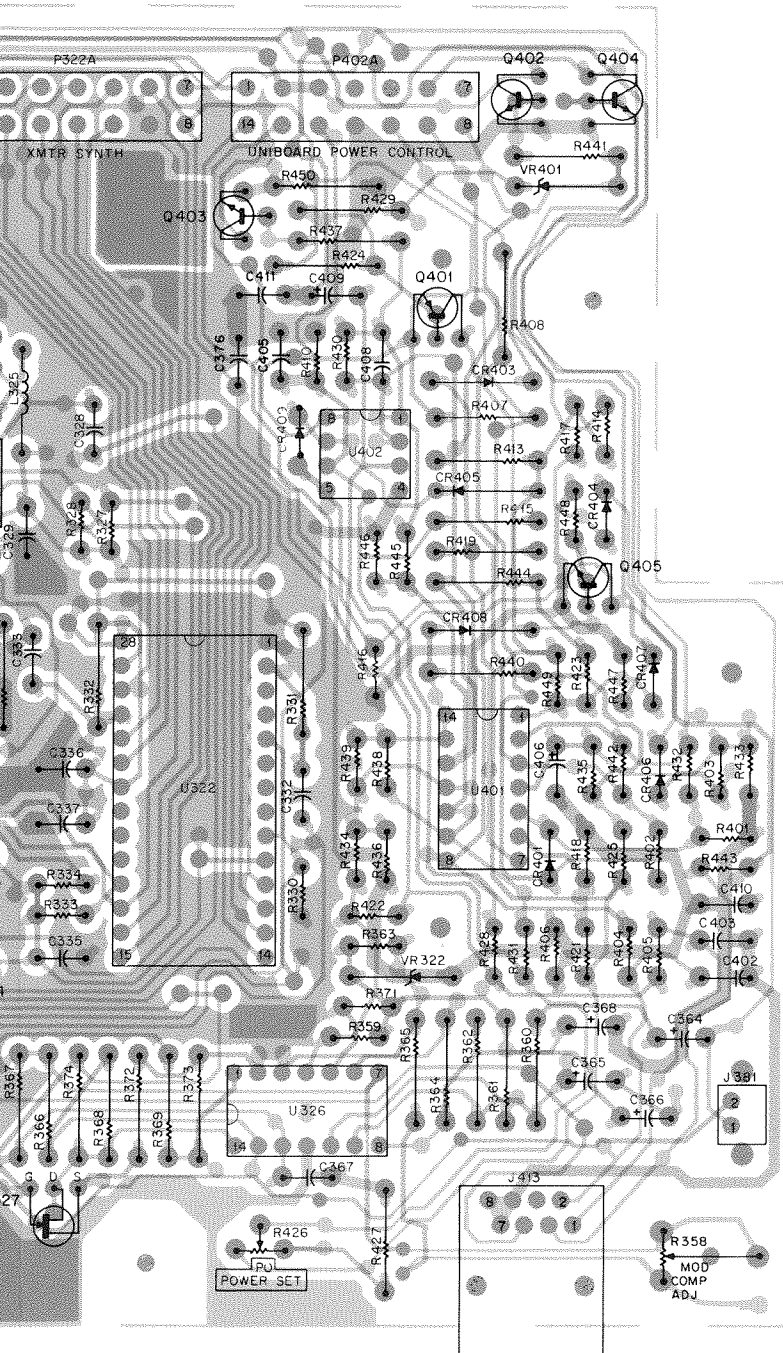


SOLDER SIDE ● BD-EEPS-45397-0  
 COMPONENT SIDE ○ BD-EEPS-45398-0  
 ○L-EEPS-45399-0

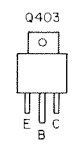
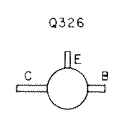
- 6-8 GND
- 5 XMTR SYNTH
- 4 STEERING LINE
- 3 NOT USED
- 2 CONTROL VOLTAGE
- 1 REFLECTED VOLTAGE
- 1 FORWARD VOLTAGE

EXT R  
 EXT R

- 11 SD 2
- 10 SD 1
- 9 AUDIO GND
- 8 +9.6V
- 7 XMIT AUDIO
- 6 SD 0
- 5 SD 3
- 4 XMIT\_LOOP
- 3 SA 0
- 2 SA 2
- 1 XMIT STROBE
- 14 PA ON
- 13 FORWARD VOLTAGE
- 12 REFLECTED VOLTAGE
- 11 AUDIO GND
- 10 HEATSINK TEMP
- 9 CIRCULATOR TEMP
- 8 PA KEY
- 7 N.C.
- 6 PA FULL POWER
- 5 N.C.
- 4 N.C.
- 3 A+
- 2 A+
- 1 PA POWER CUTBACK



Q202, Q263-Q265,  
Q322-Q325, Q401,  
Q402, Q404, Q405



EXT REF INPUT  
EXT REF MOD

DER SIDE ● BD-EEPS-45397-0  
ENT SIDE ● BD-EEPS-45398-0  
OL-EEPS-45399-0

- TX  
METERING
- 6-S GND
  - 5 XMIT SYNTH
  - 4 NOT USED
  - 3 CONTROL VOLTAGE
  - 2 REFLECTED VOLTAGE
  - 1 FORWARD VOLTAGE

# UNIBOARD

## CIRCUIT LOCATION AND INTERCONNECT DETAIL

### MODEL TRN9880A

OTOROLA PART NO.	DESCRIPTION
1498F05	HOUSING, shell
1301K03	HOUSING, 5-contact
1302K01	PLUG, key
1499F01	TERMINAL, contact; 5 used
1204N01	CABLE, 4-conductor; 6.63" lg
1717M01	CONTACT, female; 4 used
1751D89	IPA RF Input
includes:	
365D02	CONNECTOR, male; coaxial
859004	CABLE, coaxial; 6" lg
011N01	CLIP, coaxial connector
751D85	XMTR VCO RF Output
includes:	
365D02	CONNECTOR, male; coaxial
859004	CABLE, coaxial; 6" lg
crystal:(see note)	
396K08	10.796MHZ
011E05	10.7MHZ
011E05	10.7MHZ
011E05	10.7MHZ
011E05	10.7MHZ
011E05	10.7MHZ

non-referenced items	
365R01	LABEL, bar code
300B01	HANDLE
350N01	SHIELD, circuit board (top); 2 used
121N01	SHIELD, transmitter
120N02	SHIELD, circuit board (top); 2 used
122N03	SHIELD, circuit board (top); 3 used
149N01	SHIELD, circuit board (top); 2 used
122N04	SHIELD, circuit board (top)
121N03	SHIELD, transmitter
122N01	SHIELD, circuit board (top); 5 used
198N02	SHIELD, I-F
100B02	HANDLE; 7 used
23N01	SHIELD, circuit board (bottom)
26N02	SHIELD, circuit board (bottom)
25N01	SHIELD, circuit board (bottom)
100B05	HANDLE
27N01	SHIELD, circuit board (bottom)
197N01	SHIELD, transmitter (solder side)
199N02	SHIELD, transmitter
24N01	SHIELD, circuit board (bottom)
21N02	SHIELD, transmitter
49854	WASHER, spacer (used with U201)
02K01	INSULATOR, crystal; 6 used
14A01	TERMINAL, coaxial; 4 used

nance, diodes, transistors, and integrated circuits must rt numbers.

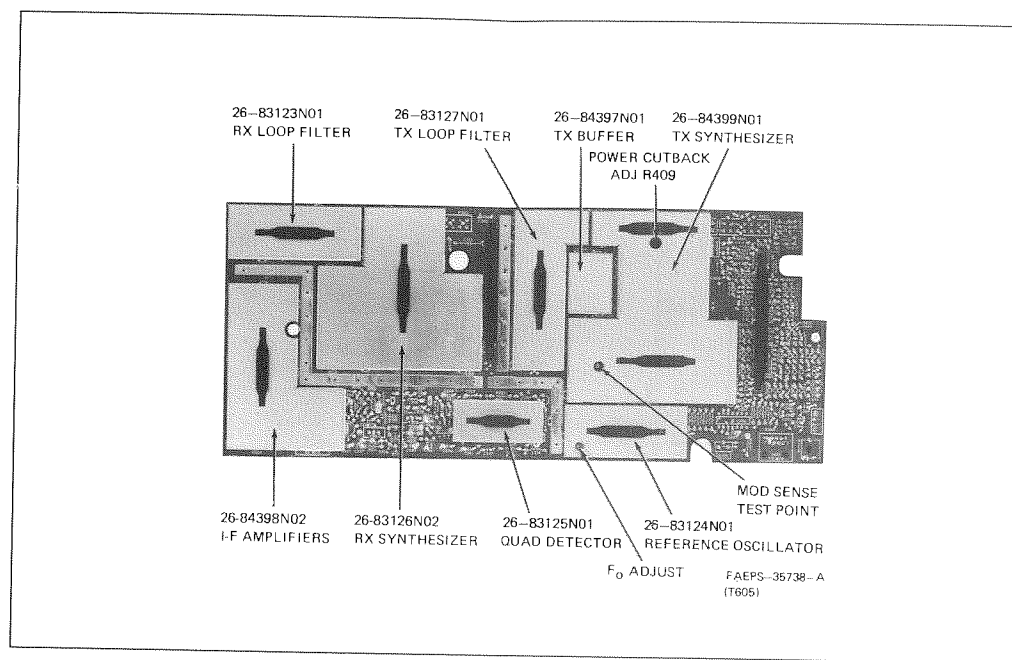


Figure 5. Uniboard Shield Detail (Solder Side)

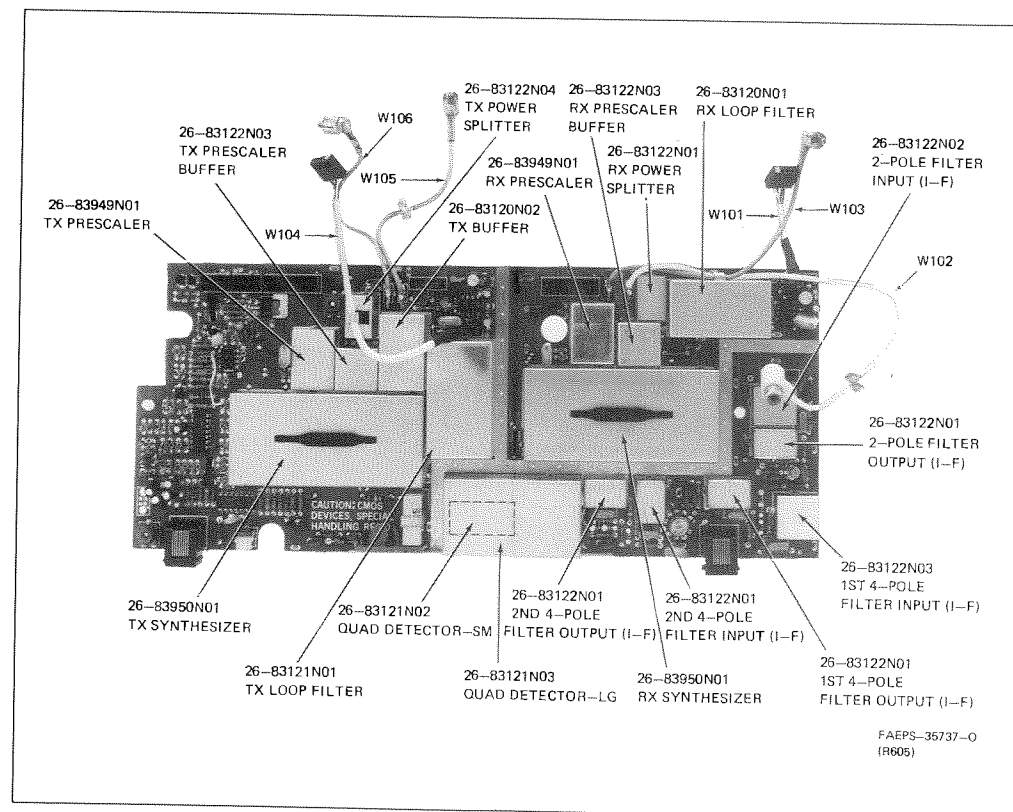


Figure 6. Uniboard Shield Detail (Component Side)

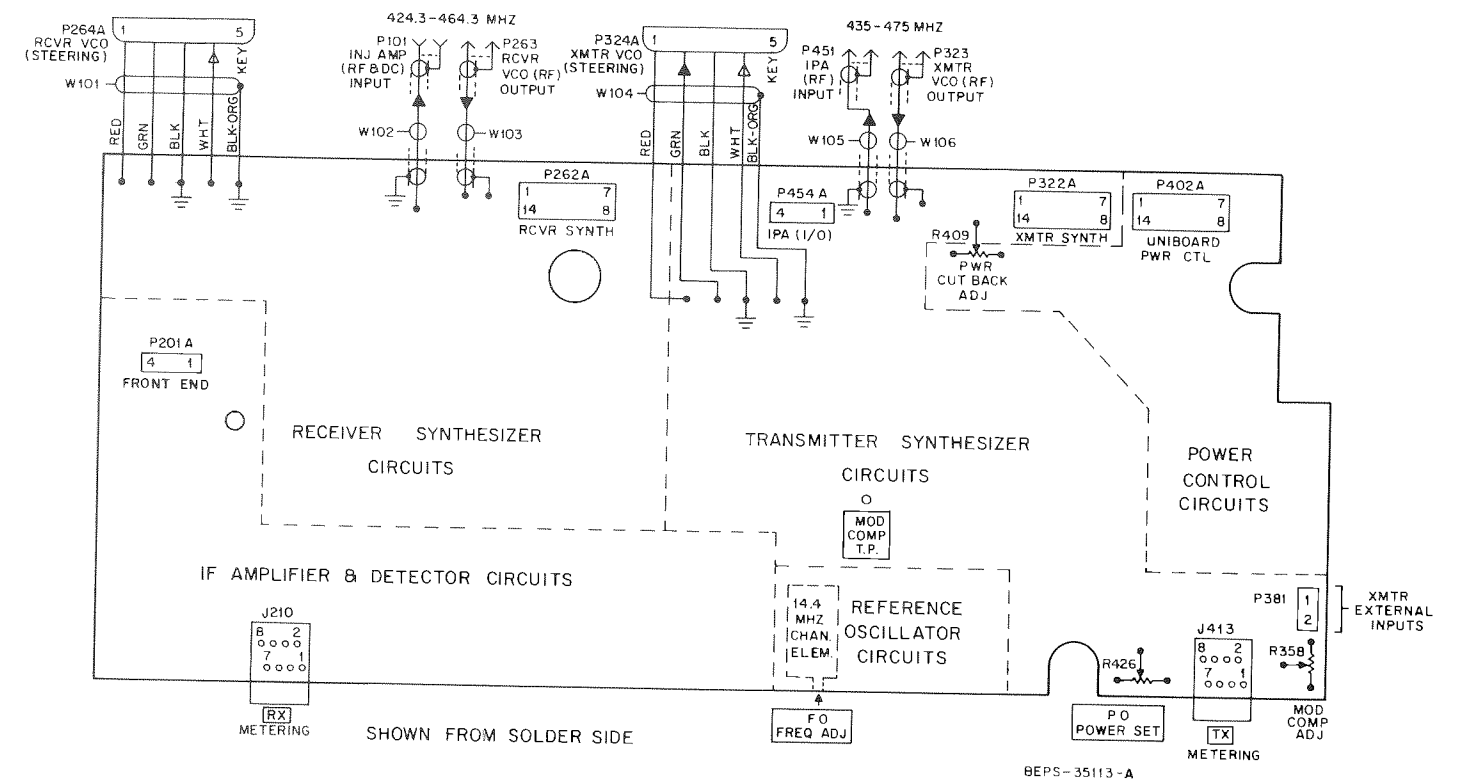


Figure 7. Uniboard Circuit Location and Interconnect Detail

REFER TO APPROPRIATE MANUAL SECTION FOR SCHEMATIC DIAGRAMS AND CIRCUIT BOARD DETAILS



# parts list

TRN9880A Uniboard

PL-10850-O

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION	REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
		capacitor, fixed: $\mu\text{F} \pm 5\%$ ; 100V unless otherwise stated			
C201	2384538G06	47 $\pm 20\%$ ; 20V	C355 thru 358	2111014H32	20pF
C202	2111014H50	110pF	C359	0811044A27	0.1; 50/63V
C203	2111014H27	12pF	C360	2311019A20	10 $\pm 20\%$ ; 25V
C204	2182450B62	0.2pF; 500V	C361	2311054L14	4.7 $\pm 10\%$ ; 50V
C205	2111014H20	6.2pF $\pm .5\text{pF}$	C362,363	2311019A40	47 $\pm 20\%$ ; 25V
C207,208	0811044A24	.01; 63V	C364	2311019A20	10 $\pm 20\%$ ; 25V
C209	2111014H25	10pF $\pm .5\text{pF}$	C365,366	2311054H08	10 $\pm 10\%$ ; 25V
C210	0811044A24	.01; 63V	C367	0811044A24	.01; 63V
C211	2111014H27	12pF	C368	2311019A20	10 $\pm 20\%$ ; 25V
C212	2182450B44	0.82; 500V	C369	2311019A46	100 $\pm 20\%$ ; 25V
C215	2182450B07	0.39pF; 500V	C370,371	2111014H32	20pF
C216	2111014H13	3.3pF $\pm .25\text{pF}$	C372	0811044A24	.01; 63V
C217	2111014H32	20pF	C376	0811044A30	0.33; 50/63V
C218	2111014H30	16pF	C381,382	0811044A24	.01; 63V
C219	2111014H28	13pF	C384	2111014H25	10pF $\pm .5\text{pF}$
C220	0811044A24	.01; 63V	C402,403	2111014H38	36pF
C221	0811044A27	0.1; 50/63V	C405	0811044A24	.01; 63V
C222,223,224	0811044A24	.01; 63V	C406	2311054K06	1.0 $\pm 20\%$ ; 50V
C225	2111014H33	22pF	C408	0811051A03	.0022; 63V
C226	2111014H29	15pF	C409	2311054L04	0.68 $\pm 10\%$ ; 50V
C227	2182450B61	1pF; 500V	C410	2111014H38	36pF
C230	2182450B29	0.51; 500V	C411	0811044A12	.047; 63V
C231	2111014H38	36pF			diode:(see note)
C232	2111014H42	51pF	CR261	4883329G02	silicon
C233,234,235	0811044A24	.01; 63V	CR262	4882139G01	germanium
C236	0811044A27	0.1; 50/63V	CR321	4883329G02	silicon
C237	2111014H22	7.5pF $\pm .5\text{pF}$	CR401	4883654H01	silicon
C239	2111014H20	6.2pF $\pm .5\text{pF}$	CR403	4811034A01	silicon
C240 thru 244	0811044A24	.01; 63V	CR404	4883654H01	silicon
C245,246	2111015B05	220pF $\pm 10\%$	CR405	4811034A01	silicon
C247,248	0811044A24	.01; 63V	CR406,407	4883654H01	silicon
C249	2311054H08	10 $\pm 10\%$ ; 25V	CR408	4811034A01	silicon
C250,251,252	0811044A24	.01; 63V	CR409	4883654H01	silicon
C253	2111014H05	1.5pF $\pm .25\text{pF}$			connector:
C261	2111014H32	20pF	J210	0983112N02	female, 8-contact
C262	2111014H08	2pF $\pm .25\text{pF}$	J413	0983112N02	female, 8-contact
C263,264,265	2111014H32	20pF			coil:
C266	0811044A27	0.1; 50/63V	L201	7683960B01	ferrite bead
C267	2111014H32	20pF	L202	2411047B31	1.8UH
C268	0811044A27	0.1; 50/63V	L203	2411047C53	15UH
C269,270	2111014H32	20pF	L204	2482549D24	15UH
C271	2111015B05	220pF $\pm 10\%$	L205,206,207	2411047C53	15UH
C272	0811051A03	.0022; 63V	L208	2482723H35	23UH (red)
C273,274	2111015B05	220pF $\pm 10\%$	L209,210	2411047C53	15UH
C275, 276	0811044A27	0.1; 50/63V	L211	2482723H35	23UH (red)
C277	2111015B05	220pF $\pm 10\%$	L212	2411047B58	24UH
C278	0811044A24	.01; 63V	L213	2482549D24	15UH
C279	2311019A40	47 $\pm 20\%$ ; 25V	L261	2411030A06	86.6NH (violet)
C280	2111014H49	100pF	L262	2411030A02	21.3NH (orange)
C281,282	2111014H32	20pF	L263	2482723H28	0.29 UH (yellow)
C283	0811051A06	.0068; 63V	L264	2411030C05	choke (green)
C284	2311019A40	47 $\pm 20\%$ ; 25V			
C285	0811051A01	.001; 63V	L265 thru		
C286	0811051A05	.0047; 63V	268,275	2482723H33	14UH (orange)
C288	0811051A01	.001; 63V	L276	2411030A06	86.6NH (violet)
C289	0811044A24	.01; 63V	L278	2482835G32	0.6UH (blue/yellow/silver)
C290	2111014H32	20pF	L321	2411030A06	86.6NH (violet)
C291	0811044A24	.01; 63V	L322	2411030A02	21.3NH (orange)
C292	2311013F03	0.15 $\pm 10\%$ ; 35V	L323	2482723H28	0.29 UH (yellow)
C293	0811044A32	0.68; 50/63V	L324	2411030C05	choke (green)
C294	0811044A12	.047; 63V	L325,326,327	2482723H33	14UH (orange)
C295	0811044A24	.01; 63V	L328	2482723H28	0.29 UH (yellow)
C296,298	2111014H32	20pF	L329	2411030A02	21.3NH (orange)
C305	0811044A27	0.1; 50/63V	L330,331,381,382,383	2482723H33	14UH (orange)
C306	2311019A20	10 $\pm 20\%$ ; 25V			connector:
C307	2311054L14	4.7 $\pm 10\%$ ; 50V	P201A	0983109N02	female, 4-contact
C308	2311019A49	150 $\pm 20\%$ ; 16V	P262A	0983110N01	female, 14-contact
C309	2111014H32	20pF	P264A	2883441F05	male, 5-contact
C310	0811044A24	.01; 63V	P322A	0983110N01	female, 14-contact
C311,313,321	2111014H32	20pF	P324A	2883441F05	male, 5-contact
C322	2111014H08	2pF $\pm .25\text{pF}$	P402A	0983110N01	female, 14-contact
C323,324,325	2111014H32	20pF	P454A	0983109N02	female, 4-contact
C326	0811044A27	0.1; 50/63V			transistor:(see note)
C327	2111014H32	20pF	Q201	4800869687	MOSFET
C328	0811044A27	0.1; 50/63V	Q202	4800869643	PNP
C329,330	2111014H32	20pF	Q261	4800869839	JFET
C331	2111015B05	220pF $\pm 10\%$	Q262,263	4800869643	PNP
C332	0811051A03	.0022; 63V	Q264	4800869642	PNP
C333,334	2111015B05	220pF $\pm 10\%$	Q265	4800869681	PNP
C335,336	0811044A27	0.1; 50/63V	Q321	4800869839	JFET
C337	2111015B05	220pF $\pm 10\%$	Q322,323	4800869643	PNP
C338	0811044A24	.01; 63V	Q324	4800869642	PNP
C339	2311019A40	47 $\pm 20\%$ ; 25V	Q325	4800869681	PNP
C340	2111014H49	100pF	Q326	4884411L83	PNP
C341	2111014H32	20pF	Q327	4800869725	JFET
C343	0811051A06	.0068; 63V	Q401	4800869643	PNP
C344	2311019A40	47 $\pm 20\%$ ; 25V	Q402	4800869642	PNP
C345	0811051A01	.001; 63V	Q403	4800869640	PNP
C346	0811051A05	.0047; 63V	Q404,405	4800869642	PNP
C348	2183162H07	.002 $\pm 10\%$ ; 50V			resistor, fixed: $\pm 5\%$ ; 1/4W unless otherwise stated
C349	0811044A24	.01; 63V	R201	0611009A63	3900
C350	2111014H32	20pF	R202,203	0611009A73	10K
C351	0811044A24	.01; 63V			
C352	2311054L02	0.47 $\pm 10\%$ ; 50V			
C353	0883862M02	2 $\pm 10\%$			
C354	0811044A26	.022; 63V			

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
R204	0611009A17	47
R205	0611009A41	470
R206	0611009A91	56K
R207	0611009A41	470
R208	0611009A87	39K
R209	0611009A41	470
R210	0611009A29	150
R211	0611009A91	56K
R212	0611009A41	470
R213	0611009A87	39K
R214	0611009A45	680
R215	0611009E49	1000
R216	0611009E65	4700
R218	0611009B04	180K
R219	0611009A99	120K
R220	0611009A49	1000
R221	0611009E79	18K
R222	0611009A47	820
R223	0611009A99	120K
R224	0611009A25	100
R225	0611009E89	47K
R226	0611009A33	220
R250	0611009A17	47
R251	0611009A33	220
R261	0611009A25	100
R262	0611009A17	47
R263	0611009A25	100
R264	0611009A19	56
R265	0611009A73	10K
R266	0611009A49	1000
R267,268	0611009E65	4700
R269	0611009A41	470
R270	0611009E65	4700
R271	0611009A41	470
R272	0611009A49	1000
R273	0611009E67	5600
R274	0611009A65	4700
R275	0611009A01	10
R276	0611009A29	150
R277	0611009A39	390
R278	0611009A33	220
R279	0611009A89	47K
R280	0611009A01	10
R281	0611009A56	2000
R282	0611009A59	2700
R283	0611009A92	62K
R284	0611009B05	200K
R285	0611009A71	8200
R286	0611009A61	3300
R293	0611009A81	22K
R295	0611009A99	120K
R321	0611009A25	100
R322	0611009A17	47
R323	0611009A25	100
R324	0611009A19	56
R325	0611009A73	10K
R326	0611009A49	1000
R327,328	0611009E65	4700
R329	0611009A41	470
R330	0611009E65	4700
R331	0611009A41	470
R332	0611009A49	1000
R333	0611009E67	5600
R334	0611009E65	4700
R335	0611009A01	10
R336	0611009A29	150
R337	0611009A39	390
R338	0611009A33	220
R339	0611009A89	47K
R340	0611009A01	10
R341	0611009A56	2000
R342	0611009A59	2700
R343	0611009B18	680K
R344	0611009B05	200K
R345	0611009A77	15K
R346	0611009A61	3300
R347	0611009A11	27
R348	0611009E56	2000
R349	0611009A14	36
R350	0611009A11	27
R351	0611009A67	5600
R352	0611009E58	2400
R353	0611009E35	270
R357	0611009A73	10K
R358	1884248R09	variable; 10K 20 1/2W
R359	0611009E41	470
R360	0611009A99	120K
R361	0611009A92	62K
R362	0611009A99	120K
R363	0611009E32	200
R364	0611009A33	220
R365	0611009A49	1000
R366	0611009A73	10K
R367	0611009A81	22K
R368	0611009A73	10K
R369	0611009A71	8200
R370	0611009A99	120K
R371	0611009E65	4700

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
R372	0611009A73	10K
R373	0611009A80	20K
R374	0611009A99	120K
R381	0611009A25	100
R401	0611009E81	22K
R402	0611009E49	1000
R403	0611009E09	22
R404	0611009E97	100K
R405	0611009E99	120K
R406	0611009E49	1000
R407	0611009A61	3300
R408	0611009A64	4300
R409	1884248R09	variable; 10K 20 1/2W
R410	0611009E73	10K
R413	0611009A29	150
R414	0611009E49	1000
R415	0611009A81	22K
R416	0611009E73	10K
R417	0611009E65	4700
R418	0611009E97	100K
R419	0611009A42	510
R421	0611009E66	5100
R422	0611009E97	100K
R423	0611009E65	4700
R424	0611009A73	10K
R425	0611009E69	6800
R426	1884248R26	variable; 10K 20 1/2W
R427	0611009A49	1000
R428	0611009E65	4700
R429	0611009A57	2200
R430	0611009E97	100K
R431	0611009E81	22K
R432	0611009E93	68K
R433,434	0611009E73	10K
R435	0611009E81	22K
R436	0611009E66	5100
R437	0611009A57	2200
R438,439	0611009F18	680K
R440	0611009A65	4700
R441	0611009A73	10K
R442	0611009E69	6800
R443	0611009F18	680K
R444	0611009B06	220K
R445,446	0611009E65	4700
R447,448	0611009E73	10K
R449	0611009F06	220K
R450	0611009A01	10
RT261	0600858402	thermistor: 1K @25C
RT321	0600858402	1K @25C
U201	5183629M47	integrated circuit;(see note) Operational Amplifier
U202	5184561L84	Operational Amplifier
U261	5180235C10	Limiting/Quadrature Detector
U262	5184768F63	Prescaler
U263	5183977M36	Divider
U264	5184887K84	Phase Detector
U265	5184768F65	Quad Analog Gate
U321	5180235C10	Super Filter
U322	5184768F63	Prescaler
U323	5183977M36	Divider
U324	5184887K84	Phase Detector
U325	5184768F65	Quad Analog Gate
U326	5184621K32	Super Filter
U381	5180291B02	Quad Op Amplifier
U401	5184621K74	Oscillator
U402	5184621K89	Quad Comparator Dual Op Amplifier
VR322	4882256C03	voltage regulator: (see note) 4.7V
VR401	4882256C15	5.1V
W101	0180711E54	cable assembly: Receiver VCO Steering includes: HOUSING, shell HOUSING, 5-contact PLUG, key TERMINAL, contact; 5 used CABLE, 4-conductor; 3" lg CONTACT, female; 4 used
W102	0180751D84	Injection Amplifier RF & DC Input includes:
3084158N01	CABLE, coaxial (incls connector P101)	
W103	4284011N01 0180751D87	CLIP, coaxial connector RCVR VCO RF Output includes:
P263	2882365D02	CONNECT,male; coaxial
W104	3000859004 0180711E53	CABLE, coaxial; 7.25" lg XMTR VCO Steering includes:

REFER  
SYM

W105

P451

W106

P323

Y201

Y202

Y203

Y204

Y205

Y206

note: For  
be ordered

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
R372	0611009A73	10K
R373	0611009A80	20K
R374	0611009A99	120K
R381	0611009A25	100
R401	0611009E81	22K
R402	0611009E49	1000
R403	0611009E09	22
R404	0611009E97	100K
R405	0611009E99	120K
R406	0611009E49	1000
R407	0611009A61	3300
R408	0611009A64	4300
R409	1884248R09	variable; 10K 20 1/2W
R410	0611009E73	10K
R413	0611009A29	150
R414	0611009E49	1000
R415	0611009A81	22K
R416	0611009E73	10K
R417	0611009E65	4700
R418	0611009E97	100K
R419	0611009A42	510
R421	0611009E66	5100
R422	0611009E97	100K
R423	0611009E65	4700
R424	0611009A73	10K
R425	0611009E69	6800
R426	1884248R26	variable; 10K 20 1/2W
R427	0611009A49	1000
R428	0611009E65	4700
R429	0611009A57	2200
R430	0611009E97	100K
R431	0611009E81	22K
R432	0611009E93	68K
R433,434	0611009E73	10K
R435	0611009E81	22K
R436	0611009E66	5100
R437	0611009A57	2200
R438,439	0611009F18	680K
R440	0611009A65	4700
R441	0611009A73	10K
R442	0611009E69	6800
R443	0611009F18	680K
R444	0611009B06	220K
R445,446	0611009E65	4700
R447,448	0611009E73	10K
R449	0611009F06	220K
R450	0611009A01	10
RT261	0600858402	thermistor: 1K @25C
RT321	0600858402	1K @25C
U201	5183629M47	integrated circuit:(see note) Operational Amplifier
U202	5184561L84	Operational Amplifier
U261	5180235C10	Prescaler
U262	5184768F63	Divider
U263	5183977M36	Phase Detector
U264	5184887K84	Quad Analog Gate
U265	5184768F65	Super Filter
U321	5180235C10	Prescaler
U322	5184768F63	Divider
U323	5183977M36	Phase Detector
U324	5184887K84	Quad Analog Gate
U325	5184768F65	Super Filter
U326	5184621K32	Quad Op Amplifier
U381	5180291B02	Oscillator
U401	5184621K74	Quad Comparator
U402	5184621K89	Dual Op Amplifier
VR322	4882256C03	voltage regulator: (see note) 4.7V
VR401	4882256C15	5.1V
W101	0180711E54	cable assembly: Receiver VCO Steering includes: 1583498F05 HOUSING, shell 1584301K03 HOUSING, 5-contact 2884302K01 PLUG, key 2983499F01 TERMINAL, contact; 5 used 3084204N01 CABLE, 4-conductor; 3" lg 3982717M01 CONTACT, female; 4 used 0180751D84 Injection Amplifier RF & DC Input includes:
3084158N01	CABLE, coaxial (incls connector P101)	
W103	4284011N01 0180751D87	CLIP, coaxial connector RCVR VCO RF Output includes:
P263	2882365D02 3000859004	CONNECT,male; coaxial CABLE, coaxial; 7.25" lg
W104	0180711E53	XMTR VCO Steering includes:

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
	1583498F05	HOUSING, shell
	1584301K03	HOUSING, 5-contact
	2884302K01	PLUG, key
	2983499F01	TERMINAL, contact; 5 used
	3084204N01	CABLE, 4-conductor; 6.63" lg
	3982717M01	CONTACT, female; 4 used
W105	0180751D89	IPA RF Input includes:
P451	2882365D02 3000859004	CONNECTOR,male; coaxial CABLE, coaxial; 6" lg
W106	4284011N01 0180751D85	CLIP, coaxial connector XMTR VCO RF Output includes:
P323	2882365D02 3000859004	CONNECTOR,male; coaxial CABLE, coaxial; 6" lg  crystal:(see note)
Y201	4884396K08	10.796MHZ
Y202	9180011E05	10.7MHZ
Y203	9180011E05	10.7MHZ
Y204	9180011E05	10.7MHZ
Y205	9180011E05	10.7MHZ
Y206	9180011E05	10.7MHZ
non-referenced items		
	5483865R01	LABEL, bar code
	5584300B01	HANDLE
	2683950N01	SHIELD, circuit board (top); 2 used
	2683121N01	SHIELD, transmitter
	2683120N02	SHIELD, circuit board (top); 2 used
	2683122N03	SHIELD, circuit board (top); 3 used
	2683949N01	SHIELD, circuit board (top); 2 used
	2683122N04	SHIELD, circuit board (top)
	2683121N03	SHIELD, transmitter
	2683122N01	SHIELD, circuit board (top); 5 used
	2684398N02	SHIELD, I-F
	5584300B02	HANDLE; 7 used
	2683123N01	SHIELD, circuit board (bottom)
	2683126N02	SHIELD, circuit board (bottom)
	2683125N01	SHIELD, circuit board (bottom)
	5584300B05	HANDLE
	2683127N01	SHIELD, circuit board (bottom)
	2684397N01	SHIELD, transmitter (solder side)
	2684399N02	SHIELD, transmitter
	2683124N01	SHIELD, circuit board (bottom)
	2683121N02	SHIELD, transmitter
	0400049854	WASHER, spacer (used with U201)
	1484602K01	INSULATOR, crystal; 6 used
	2980014A01	TERMINAL, coaxial; 4 used

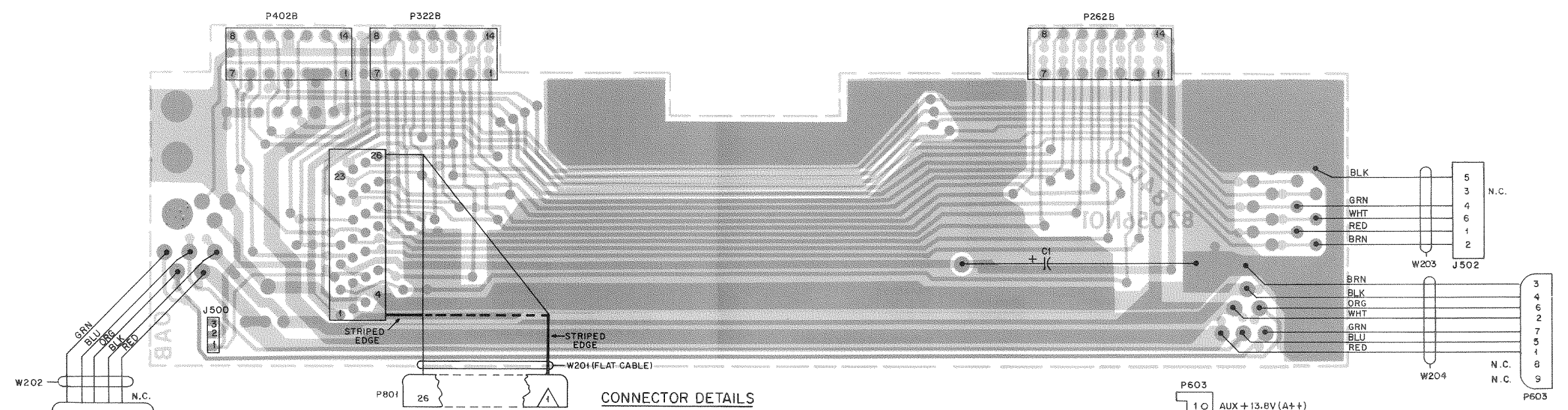
note: For optimum performance, diodes, transistors, and integrated circuits must be ordered by Motorola part numbers.



SD1 (SYNTH DATA BIT 1)	SD2 (SYNTH DATA BIT 2)	SD3 (SYNTH DATA BIT 3)	SPARE 1	SPARE 2	SPARE 3	TRANSMIT MODULATION AUDIO	TRANSMIT LOCK	TRANSMIT LOOP	TRANSMIT STROBE
9	8	6				7	12*	4*	1
10	11	5							
			5	7	4				
19*	21*	23*				3*	8	18	26*

+9.6V	1	0	2	
TRANSMIT MODULATION AUDIO	0	0	0	AUDIO GND (GND A)
RECEIVE AUDIO	0	0	0	
ANTENNA RELAY ENABLE	0	0	0	TRANSMIT LOCK
+5V	0	0	0	PA FULL POWER
LOGIC GND	0	0	0	PA ON
RECEIVE LOOP	0	0	0	PA KEY
RECEIVE LOCK	0	0	0	PA POWER CUTBACK
SD0	0	0	0	TRANSMIT LOOP
SD1	0	0	0	SA2
SD2	0	0	0	SA1
SD3	0	0	0	SA0
RECEIVE STROBE	250	0	26	TRANSMIT STROBE

P801 (PIN VIEW)  
CONNECTOR DETAIL



CONNECTOR DETAILS

P262B (PIN VIEW)

+5V	014	10	MAIN +13.8V (A+)
RECEIVE STROBE	013	20	LOGIC GND
SA2	012	30	RECEIVE AUDIO
SA1	011	40	RECEIVE LOOP
SA0	010	50	SD0
SD1	009	60	SD3
SD2	008	70	RECEIVE LOCK

P322B (PIN VIEW)

SA1	014	10	TRANSMIT STROBE
MODULATION ENABLE	013	20	SA2
TRANSMIT LOCK	012	30	SA0
SD2	011	40	TRANSMIT LOOP
SD1	010	50	SD3
AUDIO GND (GND A)	009	60	SD0
+9.6V	008	70	TRANSMIT MOD AUDIO

P402B (PIN VIEW)

PA ON	014	10	PA POWER CUTBACK
FORWARD VOLTAGE	013	20	MAIN +13.8V (A+)
REFLECTED VOLTAGE	012	30	MAIN +13.8V (A+)
AUDIO GND (GND A)	011	40	SPARE 3
HEATSINK TEMPERATURE	010	50	SPARE 1
CIRCULATOR TEMPERATURE	009	60	PA FULL POWER
PA KEY	008	70	SPARE 2

P603 (PIN VIEW)

1	0	AUX +13.8V (A++)
2	0	MAIN +13.8V (A+)
3	0	AUDIO GND (GND A)
4	0	GND B
5	0	OVERVOLTAGE ALARM
6	0	BATTERY REVERT (AC FAIL)
7	0	REMOTE EQUALIZE
8	0	N.C.
9	0	N.C.

P701 (PIN VIEW)

1	0	AUX +13.8V (A++)
2	0	PLUG KEY
3	0	OVERVOLTAGE ALARM
4	0	BATTERY REVERT (AC FAIL)
5	0	GND B
6	0	REMOTE EQUALIZE

J500 (PIN VIEW)

ANTENNA RELAY ENABLE	3	0
+9.6V	2	0
ANTENNA RELAY ENABLE	1	0

J502 (PIN VIEW)

NOT USED	6	3	N.C.
AUDIO GND (GND A)	5	2	CIRCULATOR TEMPERATURE
FORWARD VOLTAGE	4	1	HEATSINK TEMPERATURE

COMPONENT SIDE ● BD-CEPS-35395-0  
SOLDER SIDE ○ BD-CEPS-35396-0  
DL-DEPS-35397-A

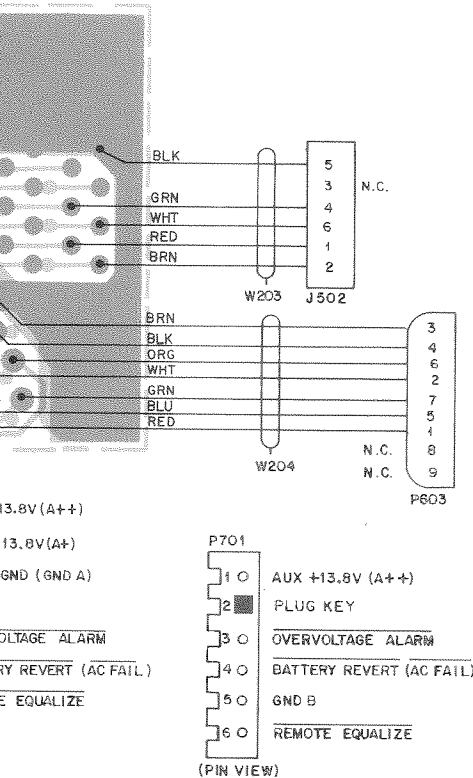
SHOWN FROM COMPONENT SIDE

# parts list

TRN5382A Interconnect Board

PL-8141-A

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
C1	23-82747L26	capacitor, fixed: 1000 uF + 100-10%; 12 V
J500	28-84315N01	connector, receptacle: 3-contact; male
J502	— 15-84954L01 29-84706E05	consists of: HOUSING, 6-position TERMINAL, crimp; 6 used
P262B, 322B, 402B P603	9-83111N02 — 9-83360N02 29-83499F01	connector, plug: 14-contact; female consists of: HOUSING; 9-position TERMINAL; contact; 7 used
P701	— 15-83498F37 29-83499F01	consists of: HOUSING, 6-position TERMINAL, contact; 5 used
P801	—	26-contact; p/o W201
W201	30-84213N01	cable, assembly: 26-conductor, flat; 9.5" used (Radio Interface); includes ref. item P801 and PCB header
W202	1-80752D19	5-conductor; 12" used (Station Control DC Power); includes ref. item P701, and
W203	1-80751D55	5-conductor; 11.25" used (PA Power Control); includes ref. item J502
W204	1-80752D20	7-conductor; 48" used (Main Power Supply); includes ref. item P603
<b>non-referenced items</b>		
	3-83498N10	SCREW, tapping; slotted star; 2 used
	7-83104N01	BRACKET, board mounting; 2 used
	42-10217A02	STRAP, tie; 3 used



TRN5142A RF Tray Hardware Kit

PL-8252-A

REFERENCE SYMBOL	MOTOROLA PART NO.	DESCRIPTION
A201	1-80752D47 7-83162N01 91-84012M03 91-84012M06	cable: I-F RF tray feedthru plate, includes: J201 A and B SUPPORT, feedthru 4 pin FILTER, RF1; 2 used
A261	1-80752D14 7-83164N01 91-84012M06	receiver synth. RF tray feedthru plate includes: J262A and B SUPPORT, feed-thru 14 pin FILTER, RF1; 14 used
A321	1-80752D15 7-83162N01 91-84012M06	IPA RF tray feedthru plate includes: J454A and B SUPPORT, feedthru 4 pin FILTER, RF1; 4 used
A401	1-80752D23 7-83143N01 64-83161N01 91-84012M06	RF tray feedthru plate xmtr synth in- cludes: J322A and B, J402A and B SUPPORT, feedthru 28 pin PLATE, mag. 2 spacer FILTER, RF1; 28 used
<b>mechanical parts</b>		
	3-10943M17	SCREW, tapping TT3.5 x 0.6 x 13"; 19 used
	3-10943M60	SCREW, tapping TT3.5 x 0.6 x 8; 3 used
	3-83498N10	SCREW, tapping M3.5 x 0.6 x 8; 6 used
	15-83133N02	TRAY, rod cost
	15-83176N01	COVER, LL amplifier core
	15-83176N02	COVER, LL amplifier core
	15-83180N01	COVER, rod tray
	32-82796H02	GASKET
	42-10217A10	CLAMP cable
	42-82387D08	CLAMP cable
	42-83501N01	RETAINER, E ring
	42-83501N02	RETAINER, E ring
	42-84244N01	CLAMP, wire tie; 2 used
	45-83153N01	CAM, 1 1/4 turns lock; 2 used
	47-83154N01	BAR, control support
	55-83354M01	HANDLE, power supply
	64-83159N01	PANEL, front



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## 1. INTRODUCTION

The *MSF 5000* transmit frequency synthesizer generates the transmit carrier. The synthesizer employs a phase-locked loop (PLL) to lock a voltage-controlled oscillator (VCO) to a reference oscillator to produce the desired frequency. Major functional blocks which are located on the uniboard, are: a 14.4 MHz reference oscillator, programmable divider, phase detector, and adaptive loop filter. An isolation buffer stage and DPL signal compensation circuit are included with the synthesizer circuits. The transmit VCO is a separate assembly located in the RF Tray.

## 2. THEORY OF OPERATION

### 2.1 PHASE-LOCKED LOOP OPERATION

**2.1.1** Various output frequencies are generated by the synthesizer by using a single negative-feedback loop, wherein the phase difference between two signals at the phase detector is used to control the VCO output frequency. The input waveforms compared are the reference signal and the loop pulse signal.

**2.1.2** The reference signal is created by dividing the output of a 14.4 MHz high-stability crystal oscillator down to a 5 kHz or 6.25 kHz square wave, using the reference divider. The loop pulse signal is the negative feedback component of the PLL, created by dividing the VCO rf output frequency by the programmable loop divide number,  $N$ .

**2.1.3** Both the loop and reference signals are applied to the phase detector, which issues a dc control voltage proportional to the phase difference between the loop and reference frequencies. The phase error output is passed through the adaptive loop filter, which damps the loop transient response and attenuates noise and spurs, to drive the VCO steering line. The steering line increases or decreases the VCO output frequency as its voltage level rises or falls. If, for instance, the VCO output frequency increases, the loop signal frequency also increases, causing a phase change at the phase detector. The phase detector then drops its dc output in accord-

ance with the phase slippage, and the steering line moves the VCO frequency back down.

### 2.2 DIVIDER

**2.2.1** The 14.4 MHz signal produced by the reference oscillator is acted upon by the programmable reference divider in U322. The internal bits  $R_1$  and  $R_2$  in U322 determine the reference signal frequency (5 kHz or 6.25 kHz).

**2.2.2** The VCO output frequency is divided by the programmable loop divider to produce the loop pulse signal. The divisor,  $N$ , is created by two dual modulus dividers. The first is a divide-by-3 or -4 prescaler U321. With the rising edge of the loop pulse signal, this prescaler divides the VCO frequency by four for 1, 2, or 3 counts of its internal "C" counter programmed by the  $C_1$  and  $C_0$  bits latched from U322. When the prescaler's "C" counter reaches zero, the VCO frequency is divided by three for the rest of the cycle which restarts with the rising edge of the next loop pulse. When the loop pulse goes low, the "C" counter is reset for the next cycle.

**2.2.3** The other dual modulus divider, divides by 63 or 64 and is located, along with the reference divider, in U322. Divide-by-64 is started with the rising edge of the loop pulse and continues until the internal "A" counter reaches zero. The loop pulse is then sent low and the divider divides by 63 until the internal "B" counter goes to zero. The loop pulse then goes high and another cycle begins. If no input signal is seen from the divide-by-3 or -4 prescaler, then U322 issues a free-running loop pulse.

### 2.3 SYNTHESIZER PROGRAMMING FROM MICROPROCESSOR

**2.3.1** For data loading into primary divider U322, the microprocessor reads data from the code plug on the station control board, and multiplexes the information into six 4-bit words. Each word is loaded into U322 as four lines of data ( $SD_0$  through  $SD_3$ ) and a corresponding three lines of address ( $SA_0$  through  $SA_2$ ), so that the words are properly demultiplexed in U322.

**2.3.2** The received data bits inform primary divider U322 and divide-by-3 or 4 prescaler U321 of the appropriate numbers for the "A", "B", and "C" counters for the desired PLL output frequency. The data bits also program the synthesizer to disable or enable its DPL modulation compensation signal or to go into its "change frequency" mode for fast lock.

## 2.4 PHASE DETECTOR

**2.4.1** Phase detector U323 issues a dc output signal proportional to the phase difference between the reference and loop pulse signals sent from divider U322. The phase difference is measured by the phase detector. It turns ramp current source Q322 on when the reference signal goes high and switches Q322 off at the leading edge of the loop pulse signal. The current generated during this interval charges C348, forming a voltage ramp.

**2.4.2** The ramp voltage is then held constant for a time interval determined by C343, allowing two hold capacitors C345 and C346 to charge to the ramp voltage level. Ramp capacitor C348 is discharged at the end of the hold interval in preparation for another ramp sequence that begins with the next reference signal leading edge.

**2.4.3** The hold capacitors are discharged through a push-pull output transistor pair via a high-to-low impedance output buffer. This creates the phase detector output signal.

**2.4.4** When the reference-to-loop-pulse phase slippage is too great for the ramp capability, the ramp remains at a high or low limit. The VCO cannot be steered to the intended frequency and an unlocked state occurs. The phase detector then issues an "adapt" signal (on the ADAPT and ADAPT lines). The ADAPT line control voltage switches the analog gates in the adaptive filter to the "normal" or "adapt" mode, as well as forcing lock indicator Q324 into a no-lock, open-collector condition. The "adapt" mode is automatically attained whenever the phase detector encounters a "change-frequency" positive pulse from U322. The duration of a single adapt duration is 12 msec, which is hard-wire controllable at the phase detector. Adapt cycles continue until reference and loop pulse signals are again locked in frequency.

**2.4.5** For fast lock, the synthesizer must be loaded when the loop pulse is low (i.e., only counter "B" is in operation). The phase detector sends a SYN THESIZER SYNC signal, at the loop pulse rate, to the microprocessor for loading synchronization.

## 2.5 ADAPTIVE LOOP FILTER

**2.5.1** The adaptive loop filter is used for effective loop lock. When the PLL is unlocked, or when a "change frequency" pulse is sent to the synthesizer from control, the ADAPT and ADAPT lines are sent high and low,

respectively, by the phase detector. Analog gates U324A, B, and C are switched closed, shorting the phase detector output to the steering line, keeping C352 uncharged, and charging C353 quickly to the new steering voltage. Gate U324D is switched open, detaching the loop filter output from the steering line. In this mode, the loop filter is essentially out of the PLL and fast lock, due to reduced damping, is possible.

**2.5.2** When the loop reaches its new frequency, (at the end of the last adapt cycle), ADAPT goes low and ADAPT goes high. Analog gates U324A, B, and C are then switched open, returning the loop filter to its normal connection to the output of U323 and breaking the direct connection between this output and the steering line. Gate U324D reconnects the loop filter output to the steering line. During this switching, C354 remains charged to the new phase detector output voltage, keeping the VCO tuned to the new frequency.

**2.5.3** The transmit loop filter, when in normal operation, has a natural frequency of 75 Hz and a third order Integral-Times-Absolute-Value-of-Error response, a method for minimization of transients. The filter damps steering line excursion due to voltage increments of the phase detector output and attenuates reference signal spurs and noise.

## 2.6 SUPER FILTER

**2.6.1** Because of the VCO requirements for a very pure dc supply voltage, an ultra-low-pass filter U325 is used to provide the VCO with a low noise +8.6 output voltage. Any ripple or noise present on the +9.6 V supply line is removed by the filter, preventing unwanted modulation of the VCO. A 1 V drop occurs across the filter. The output voltage is +8.6 V.

**2.6.2** The super filter consists of a low-pass filter, an error amplifier, and external series-pass transistor Q325. The +9.6 V supply is connected to U325-1 as well as to the emitter of Q325. Internally, the input from U325-1 passes through a low-pass filter to the noninverting input of the error amplifier. Capacitor C360, connected to U325-2, forms part of the low-pass filter. The output line (also connected to the collector of Q325) is fed back to the inverting input of the error amplifier through U325-4. The error amplifier output is connected to the base of Q325 via U325-3 and is used to control the conduction of this transistor. These connections enable the super filter to compare the output line voltage with the filtered input line voltage and to increase or decrease the conduction of Q325 to remove any ripple or noise present on the VCO supply line. The super filter output itself is filtered by C361 and C362 before being routed from the synthesizer to the VCO.



## 2.7 ISOLATION BUFFER

The isolation buffer stage applies the transmit VCO rf signal to the first stage of the intermediate power amplifier (IPA). The buffer stage consists of input and output matching circuits and an active device (Q326), biased for class A operation. The buffer ensures isolation between the VCO output and the IPA, and prevents pulling of the VCO output frequency during IPA key-up.

## 2.8 DPL MODULATION COMPENSATION

**2.8.1** The DPL modulation compensation circuit of the transmit synthesizer enables low-frequency modulation (DPL) to be transmitted without being "tracked out" by the loop. When the VCO is modulated by DPL, the modulation appears as an error signal at the phase detector, after it is divided down and compared to the reference signal. Unless compensated, this error signal passes through the loop filter and modulates the steering line, distorting the intended DPL modulation.

**2.8.2** The DPL modulation compensation circuit sends a cancellation signal to the phase detector output buffer summing point (U323-11). This cancellation signal is the original low-frequency DPL signal, after being integrated, delayed, and inverted. Thus, DPL modulation of the VCO results without loop tracking interference.

## 2.9 VOLTAGE-CONTROLLED OSCILLATOR (VCO)

**2.9.1** Each *MSF 5000* radio contains a transmit VCO that provides the frequency modulated (FM) transmit excitation frequency. The transmit VCO has a mechanical tuning range from 435 MHz to 475 MHz. Over this mechanical tuning range, the transmit VCO has an associated operational electronic bandwidth of 6.1 MHz, minimum.

### 2.9.2 Oscillator Circuit

The VCO uses a grounded-gate Colpitts oscillator that contains JFET Q26 as the amplifying element. The drain and source of the JFET are capacitively coupled to a resonant cavity via an encapsulated probe assembly. This coupling network provides the positive feedback necessary for oscillation.

### 2.9.3 Oscillator Output Amplifier/Low-Pass Filter Circuit

A second probe assembly (power output probe) is used to bring the oscillator signal out of the cavity and into output amplifier Q27. The output amplifier is a common emitter stage that is low-pass filtered. The output of the low-pass filter is then applied to the VCO's output phono connector J323. The output of the VCO

drives 10:1 power tap on the uniboard, via coaxial cable W106.

### 2.9.4 Steering Line Circuit

The steering line, in conjunction with the tuning screw, determines the VCO operating frequency. The steering line is driven by phase detector U323 and is coupled to the VCO via the adaptive loop filter. The phase detector provides a dc output voltage to maintain the VCO output at the desired frequency. When the oscillator frequency is changed, the phase detector dc output voltage shifts to change the oscillator frequency and then maintains this new frequency. The steering line is coupled from the uniboard via P324A-4 of VCO interconnect cable W104 to the VCO feedthru plate A26. This plate contains rf filters that decouple the VCO circuits from the uniboard. The steering line dc voltage determines the capacitance of diodes CR29 through CR34, which electronically control the oscillator's frequency. An increase in the steering line voltage causes the capacitance of these diodes to decrease and the oscillator frequency to increase. Conversely, a decrease in the steering line voltage causes an increase in the capacitance of the diodes and a reduction in the oscillator frequency.

### 2.9.5 Modulation Line

The VCO is directly modulated by the transmit audio signals. This is achieved by using a second varactor circuit that employs CR27 and CR28. The transmit audio signal is coupled, via P324A-2 of VCO interconnect cable W104, to CR27 whose function is to modulate the oscillator frequency. The second device, CR28, is used to maintain the modulation level constant throughout the radio operating frequency range. Without CR28, the VCO modulation sensitivity would naturally increase as the steering line increased the oscillator frequency. With CR28 in use, the series combination (of CR27 and CR28) decreases in capacitance with increasing steering line voltage, since a sample of the steering line biases CR28. Thus, modulation sensitivity is level across the VCO electronic bandwidth.

## 3. SYNTHESIZER TROUBLESHOOTING PROCEDURE

**3.1** Refer to the Transmit Frequency Synthesizer Troubleshooting Chart at the end of this section for a comprehensive procedure for troubleshooting the transmit frequency synthesizer.

**3.2** The major problems that may occur in the transmit frequency synthesizer are:

- synthesizer does not lock
- synthesizer locks on wrong frequency
- excessive reference frequency feedthrough (spurs)
- noisy frequency lock
- slow switching response.

**3.3** A summary of the problems and possible causes in the frequency synthesizer is provided in Table 1. Also refer to the other tables that provide pin connections and voltages for the phase detector, divider, prescaler, and super filter.

### **3.4 VCO TESTS**

#### **3.4.1 VCO Electronic Bandwidth Test**

Step 1. Remove the wire from P324A-4 to open the steering line. Connect a 1 kilohm resistor to the positive terminal of a 0-10 V adjustable power supply and connect the other end of the resistor to P324-A. Connect the negative terminal to VCO ground. This power supply will serve as a steering line in this test. Connect a frequency counter to VCO output connector J323.

Step 2. Adjust the power supply for 8.0 V and record the frequency.

Step 3. Adjust the power supply for 3.0 V and subtract this frequency from the frequency obtained in Step 2. The difference is the electronic bandwidth (EBW) of the VCO. The EBW should be a minimum of  $10 \pm 0.5$  MHz for the transmit VCO. If the EBW is less than specified or if the VCO does not steer at all, refer to the VCO steering line short/open test.

#### **3.4.2 Steering Line Short/Open Test**

Step 1. Check the varactor stack for a short (with an ohmmeter) by placing the positive lead on the steering line and the negative lead on the VCO ground. The reading should be greater than 20 megohms. A reading of less than 20 megohms indicates a defective or shorted component in the steering line circuit.

Step 2. Reverse the ohmmeter leads. This reading should be 500 to 1000 ohms.

Step 3. Lift one end of L30 and repeat Steps 1 and 2. If unit now passes 1 and 2, check CR28 and test EBW; otherwise, continue.

Step 4. Lift one end of L31 and one end of L32. Individually check CR29 and CR30 for a short or open and make necessary repairs.

Step 5. Reconnect L30, L31, and L32.

Step 6. Repeat Steps 3 through 5 for the following groups of varactors and chokes.

L33, L34 & CR31, CR32  
L39, L40 & CR33, CR34

Step 7. If the unit still does not pass Steps 1 and 2, remove C34 and C41, one at a time, and repeat Steps 1 and 2. If the VCO is still defective, replace the VCO.

#### **3.4.3 VCO Steering Line Leakage**

The VCO steering line leakage can be checked by removing the wire to P324A-4 and connecting one end of a 1 megohm resistor in its place. The free end of the resistor should be connected to an adjustable power supply set to 9.5 V. A high impedance voltmeter (greater than 10 megohms) should be used to verify that the voltage drop across the resistor is less than 10 mV. A higher voltage (greater than 10 mV) is an indication of either a leaky VCO feedthru assembly A26 or defective VCO steering line varactors CR29 through CR34. To determine which is defective, remove the VCO cover from the VCO and perform the same test again (with the VCO interconnect cable connected to the cover). If the voltage drop becomes less than 10 mV, the steering line varactors are leaky and need replacement. If the voltage across the resistor is still greater than 10 mV, feedthru assembly A26 is defective and requires replacement.

Table 1. Problems and Their Possible Causes in a MSF 5000 Transmit Synthesizer

Problems	Possible Source of Trouble
Synthesizer does not lock	Refer to Transmit Synthesizer Troubleshooting Chart.
Synthesizer does not lock all channels	Refer to Transmit Synthesizer Troubleshooting Chart.
Synthesizer locks on wrong frequency	Refer to Transmit Synthesizer Troubleshooting Chart.
Excessive reference frequency feedthru (spurs)	Defective hold capacitors (open or leaky) C345, C346
	Defective ramp capacitor C348.
	Defective phase detector U323.
	Adaptive filter in ADAPT mode or shorted input to output; guard band shorted to VCO steering line or other adaptive filter mode.
Noisy frequency lock	Leaky VCO varactor diodes.
	Marginal input level to prescaler U321-1, loop divider U322-25 or reference divider U322.
	Loose connection, cold solder joint, or faulty component.
	Noisy Q322.
	Defective phase detector U323.
	Defective reference divider U322 or prescaler U321 (jittery).
	Noisy 5 V or 9.6 V supplies, noisy super filter output.
	Defective adaptive filter (open capacitors).
Slow frequency switching response	Malfunctioning adaptive filter, check U324.
	Phase detector U323 gain too low (overdamped response) or too high (underdamped response); check R336, R337, R338, RT321, Q322.
	Check ramp slope at U323-24.
	Leaky adaptive filter capacitors or transmission gates C353, C352, C354 or U324.
	Leaky VCO varactor diodes.

Table 2. Phase Detector U323 Pin Connections and Voltages

Pin No.	Function	To/From	Nominal Voltage
1	high current ground	—	0 V dc.
2	REFERENCE IN	from U322-5	0 to 4.3 V square wave (160 usec period); U323-17, 5 V dc transmit.
3	adapt select	—	0 V dc
4	SYNTHESIZER SYNC	to microcomputer	60 usec positive pulse, 0-5 V at loop pulse rate; equal to pin 2 if pin 7 is low.
5	FREQUENCY CHANGE	from U322-18	0.5 V, 11.1 usec when frequency changes.
6	N.C.	—	—
7	ADAPT	to lock transistor via R339	9.6 to 0.6 V single pulse, 12 msec.
8	N.C.	—	—
9	N.C.	—	—
10	ADAPT	to adaptive filter	0 to 9 V single pulse; 12 msec Tx (U232).
11	mod input	from R369 (U323 only)	4.9 to 0.62 V dc (use high impedance).
12	HOLD 1	to C345	1.4 to 8 V dc (use high input impedance voltmeter).
13	HOLD 2	to C346	1.4 to 8 V dc (use high input impedance voltmeter).
14	A +	—	9.6 V dc
15	PHASE DET OUTPUT	to adaptive filter	1.2 to 9.5 V dc (depending on loop output frequency).
16	low current ground	—	0 V dc.
17	EXT PNP BASE	to Q323 base	8.9 V dc
18	V <sub>cc</sub>	from regulator	9.6 V dc
19	RAMP BASE	to Q322 base (ramp generator)	9.1 V dc
20	FILTERED 9.1 V	to R336, RT321, R337, C344	9.1 V dc
21	ramp resistor	to R378, U322 emitter	8 to 8.7 V dc rectangular wave at reference rate.
22	SAMPLE TIMING CAP.	to C343	0 to 2 V sawtooth wave at loop pulse rate.
23	LOOP IN PULSE	from U322-9 via C340	1.4 V pulse riding on 1.6 V dc (160 usec, typical period)
24	RAMP CAP.	from C348 and ramp Q322 collector	flat top ramp waveform at reference rate, top voltage 1.4 to 7 V (depending on loop output frequency).

Table 3. Divider U322 Pin Connections and Voltages

Pin No.	Function	To/From	Nominal Voltage
1*	GND	—	0 V dc.
2	REF IN	from U268 (reference oscillator)	1.5 V dc +0.6 V pp ac (14.4 MHz).
3	N.C.	—	—
4	N.C.	—	—
5*	REFERENCE OUT	to U323 (phase detector)	0 to 4.3 V square wave (5.0 kHz to 6.25 kHz).
6	N.C.	—	—
7	N.C.	—	—
8	N.C.	—	—
9*	LOOP OUT	to phase detector and prescaler	2.9 V to 4.3 V narrow pulse (1.4 V <sub>pp</sub> ) (160 usec nominal period).
10*	V <sub>cc</sub>	from regulator	5 V dc.
11	D0	from microcomputer	0 to 5 V pulse train.
12	D1	from microcomputer	0 to 5 V pulse train.
13	D2	from microcomputer	0 to 5 V pulse train.
14	D3	from microcomputer	0 to 5 V pulse train.
15	C0	to prescaler	0 to 5 V dc
16	C1	to prescaler	0 to 5 V dc.
17	VCO3	to Q327 gate	0 to 5 V dc.
18	FREQ CHANGE	to phase detector U323-5	0 to 5 V dc.
19	VC01	N.C.	—
20	VC02	N.C.	—
21	N.C.	—	—
22	V <sub>BB</sub>	R331, C337, R271, C277	1.5 V dc.
23	A0	from microcomputer	0 to 5 V pulse train.
24	A1	from microcomputer	0 to 5 V pulse train.
25	F <sub>IN</sub>	from prescaler U321-3	1.5 V dc +0.7 V <sub>pp</sub> ac (approx 150 MHz).
26	A2	from microcomputer	0 to 5 V pulse train.
27*	STROBE	from microcomputer	0 to 5 V pulse train (7 pulses/train).

\* should be checked first

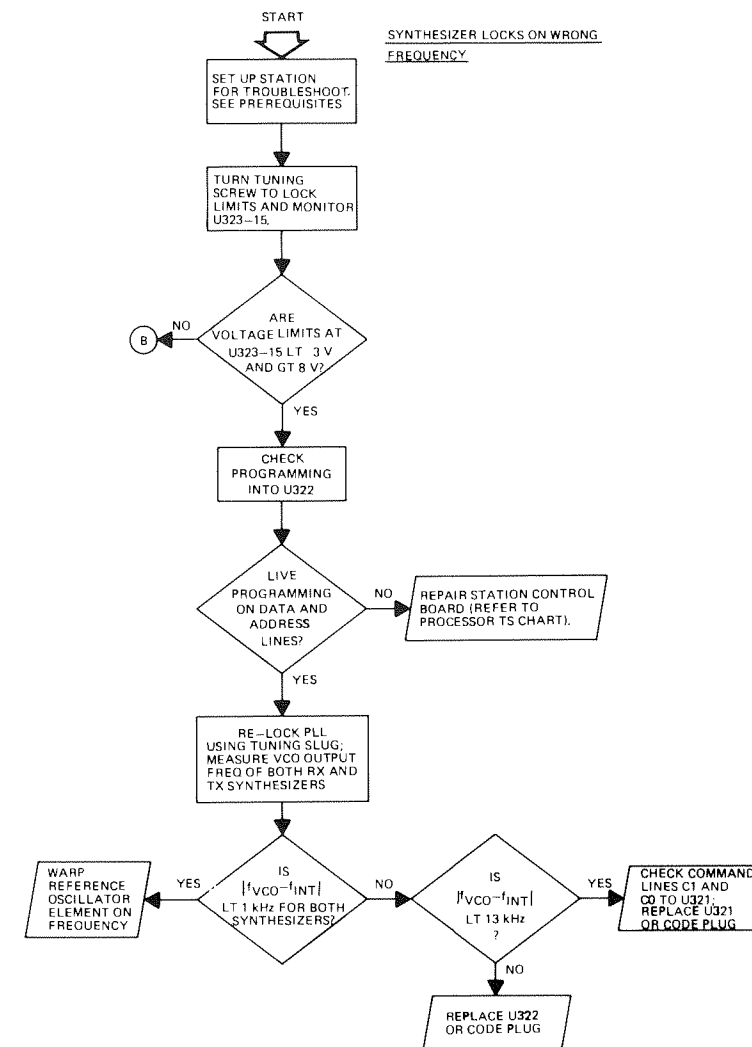
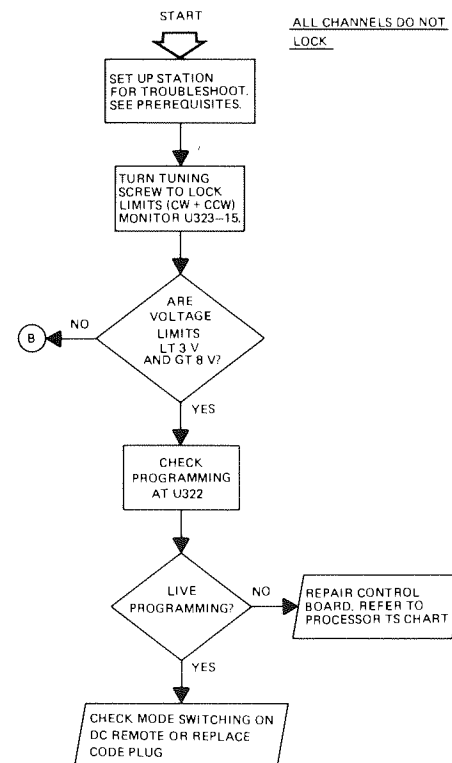
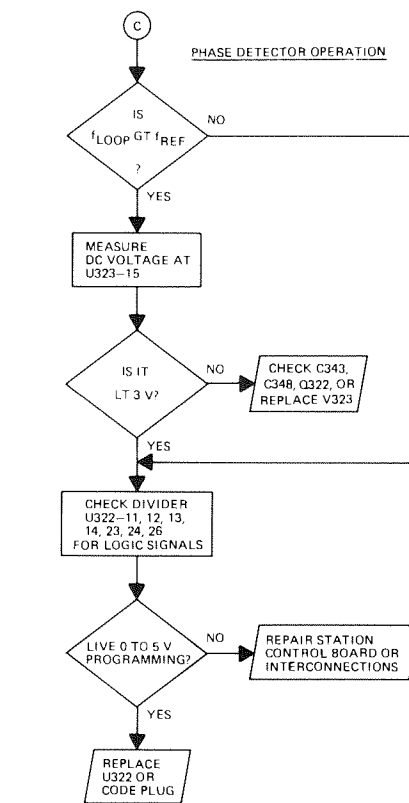
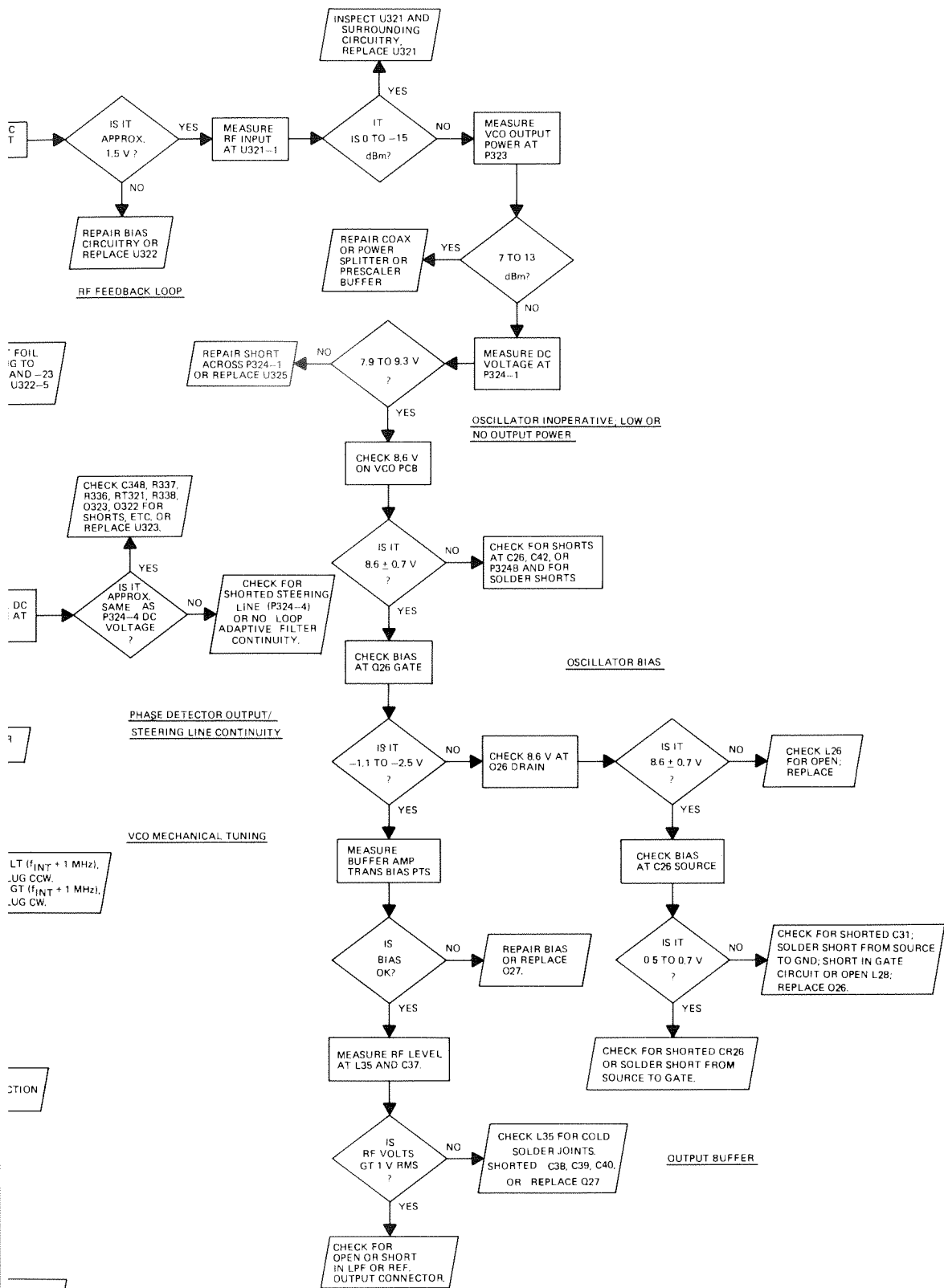
Table 4. Prescaler U321 Pin Connections and Voltages

Pin No.	Function	To/From	Nominal Voltage
1	F <sub>IN</sub>	from VCO buffer	-15 dBm to 0 dBm riding on 3.8 V dc.
2	V <sub>BB</sub>	—	3.8 V dc, bypassed for rf.
3	PRESCALER OUT	to divider U322-25	0.6 V <sub>pp</sub> riding on dc level of 3.6 V dc at approx one-third VCO freq ( $\pm 10\%$ ).
4	GND	—	0 V dc
5	F <sub>v</sub>	from divider U322-9	1.4 V <sub>pp</sub> narrow pulse at reference freq (6.25 kHz) riding on 3.4 V dc.
6	C1	from divider U322-16	dc level (programming bit) 0 or 5 V dc.
7	C0	from divider U322-15	dc level (programming bit) 0 or 5 V dc.
8	V <sub>cc</sub>	from regulator	+5 $\pm 0.1$ V

Table 5. Super Filter Pin Connections and Voltages

Pin No.	Function	To/From	Nominal Voltage
1	V <sub>cc</sub>	from 9.6 V regulator	9.6 V dc
2	FILTER CAP.	C360	7.1 V dc
3	EXT. DRIVER CONTROL	Q325	8.9 V dc
4	8.6 V OUT	to VCO	8.6 V dc
5	Ground (internal NPN emitter)	from regulator	0 V dc
6	N.C.	—	—
7	N.C.	—	—
8	N.C.	—	—

# TRANSMIT FREQUENCY SYNTHESIZER TROUBLESHOOTING CHART



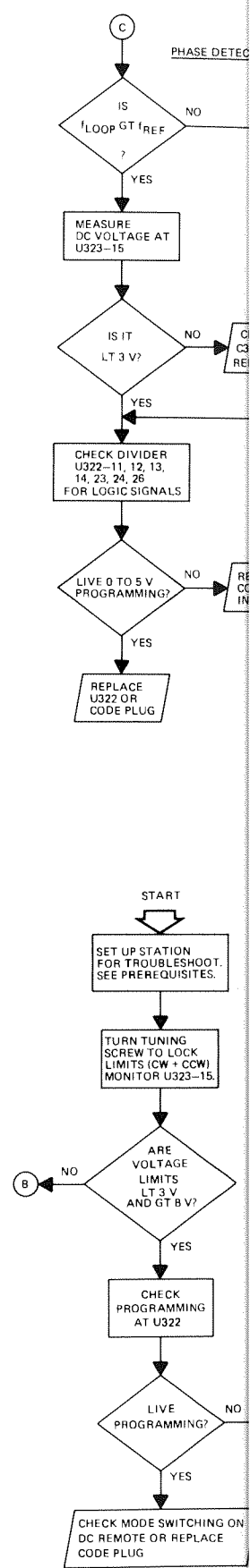
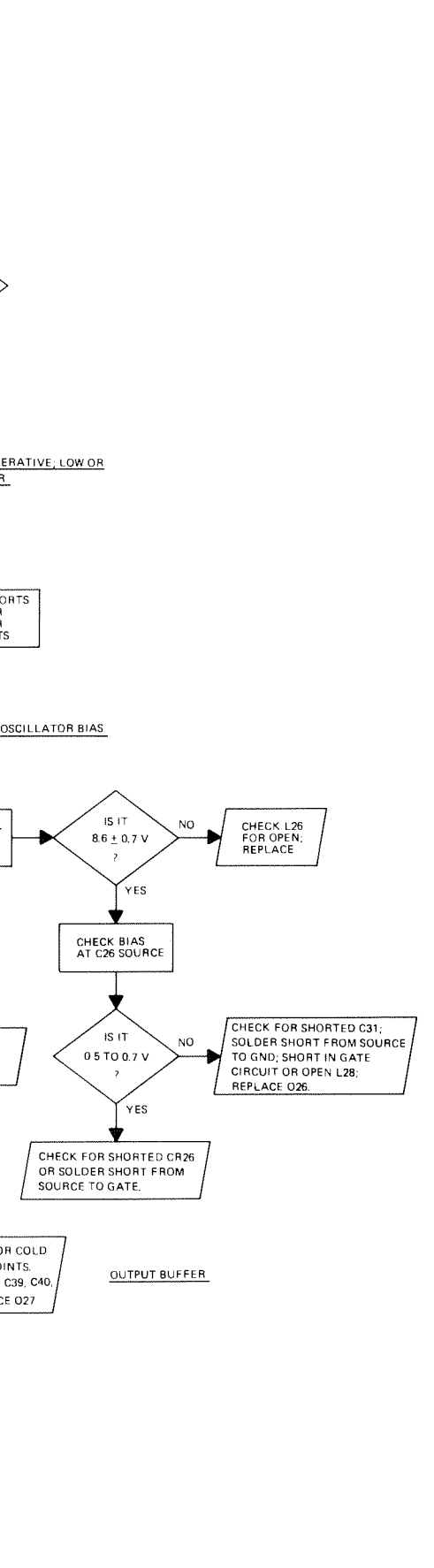
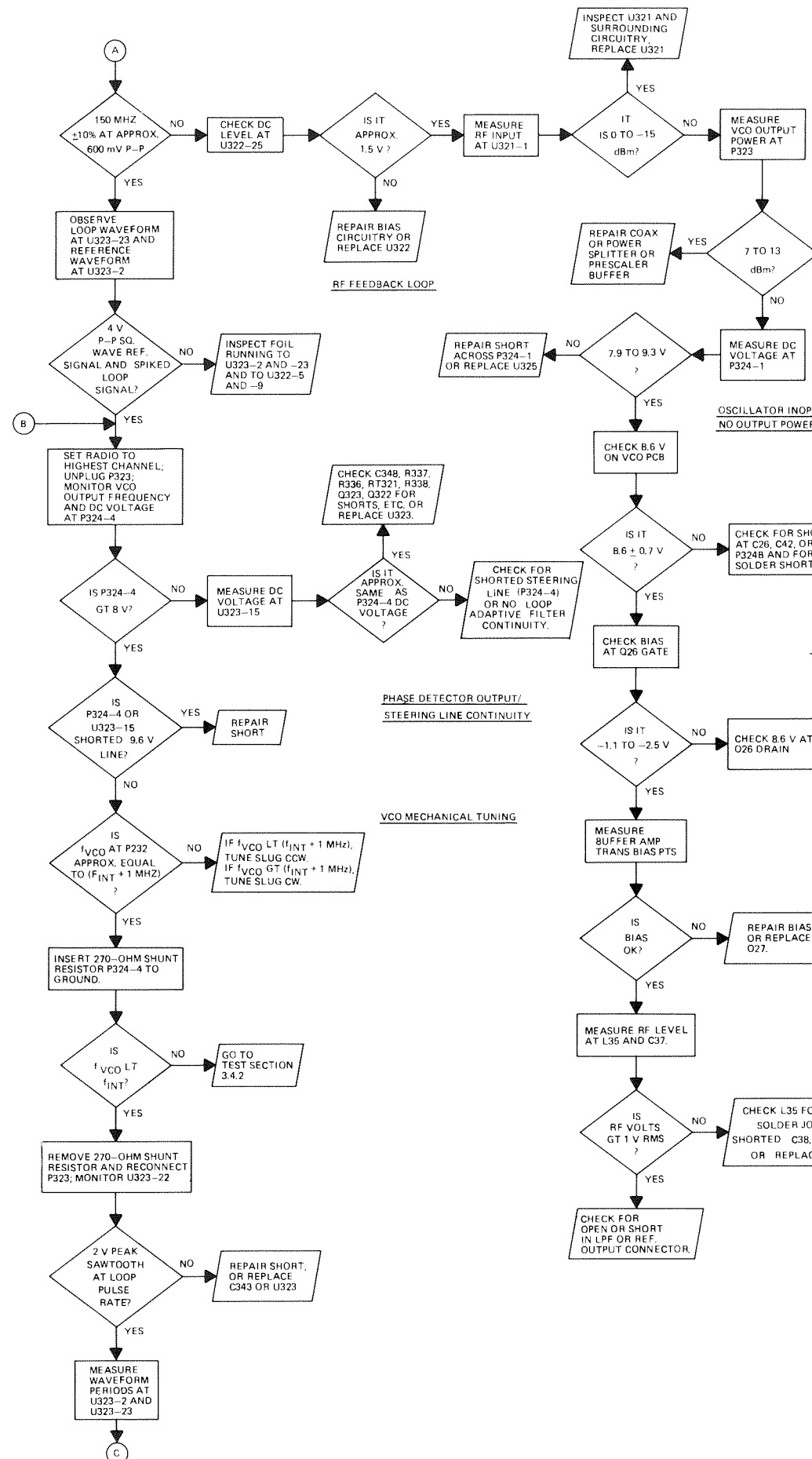
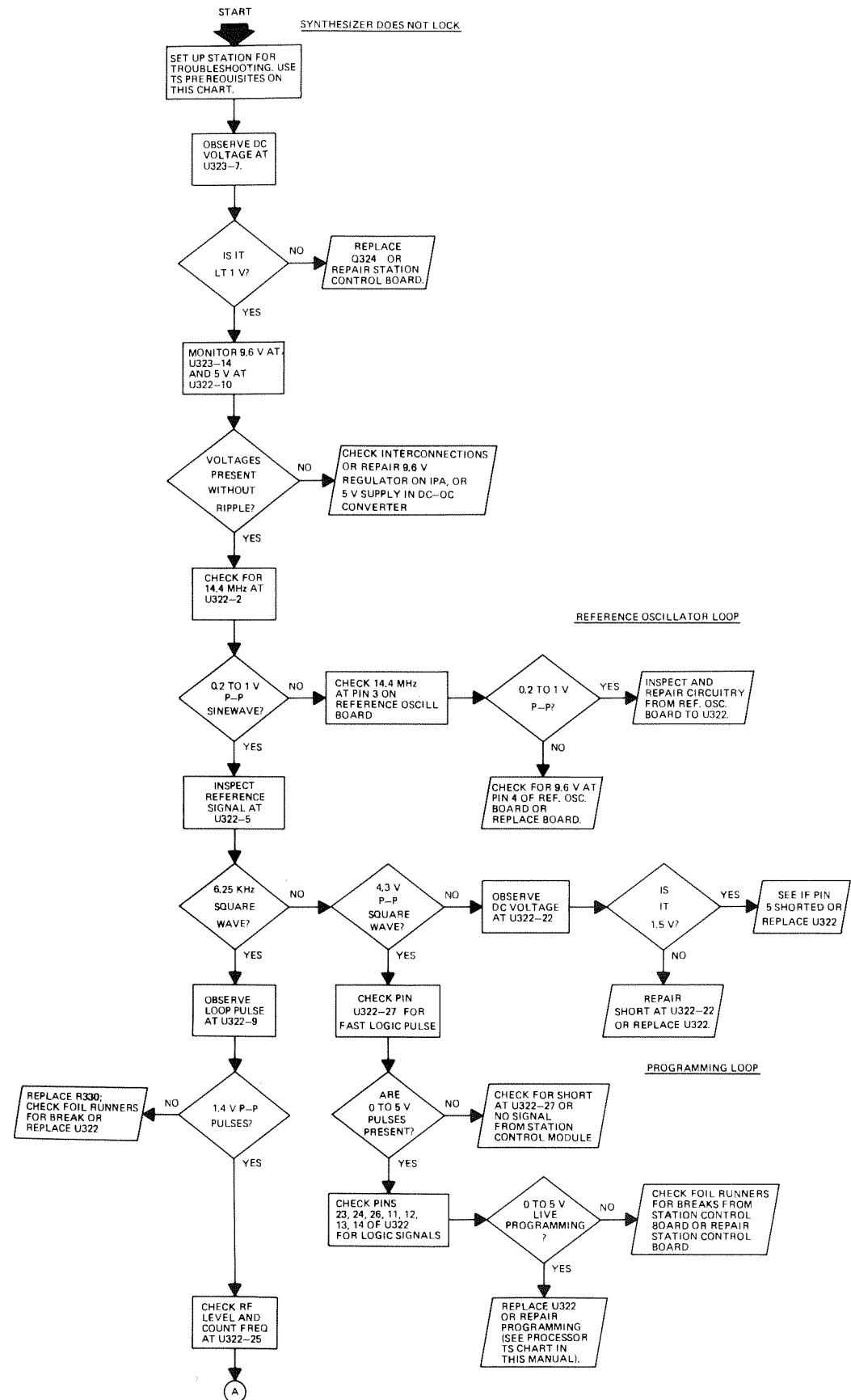
- TROUBLESHOOTING PREREQUISITES:
- THE FOLLOWING TEST EQUIPMENT IS REQUIRED FOR TROUBLESHOOTING THE SYNTHESIZER CIRCUITS: AN RF FREQUENCY COUNTER, RF PROBE, DC VOLTMETER, 30 MHz BANDWIDTH OSCILLOSCOPE, OHM METER, 270 OHM ±5%, 1/4 W RESISTOR (MOTOROLA NO. 6-11009C35), VCO TUNING TOOL, REFERENCE OSCILLATOR TUNING TOOL, AND RF POWER METER.
  - WITH STATION POWERED AND DE-KEYED, UNLATCH AND SLIDE RF TRAY OUT. TILT UP STATION CONTROL TRAY, AND THEN REMOVE RF TRAY COVER.
  - REMOVE SOLDER SIDE SHIELDS FROM MALFUNCTIONING SYNTHESIZER CIRCUIT AREA ON UNIBOARD.

SYMBOLS AND ABBREVIATIONS USED IN THE CHART

ALL VOLTAGE MEASUREMENTS ARE DC, UNLESS OTHERWISE STATED

[ ]	= TEST TO BE DONE	U323-7	= PIN NO. 7 OF U323
◇	= DECISION	P-P	= PEAK-TO-PEAK
[ ]	= SOURCE OF FAULT	$f_{VCO}$	= VCO OUTPUT FREQUENCY
		$f_{INT}$	= INTENDED FREQUENCY
		$f_L$	= LOOP PULSE FREQUENCY
		$f_R$	= REFERENCE FREQUENCY
		PCB	= PRINTED-CIRCUIT BOARD
		GT	= GREATER THAN
		LT	= LESS THAN
		TS	= TROUBLESHOOTING
		PLL	= PHASE-LOCK LOOP

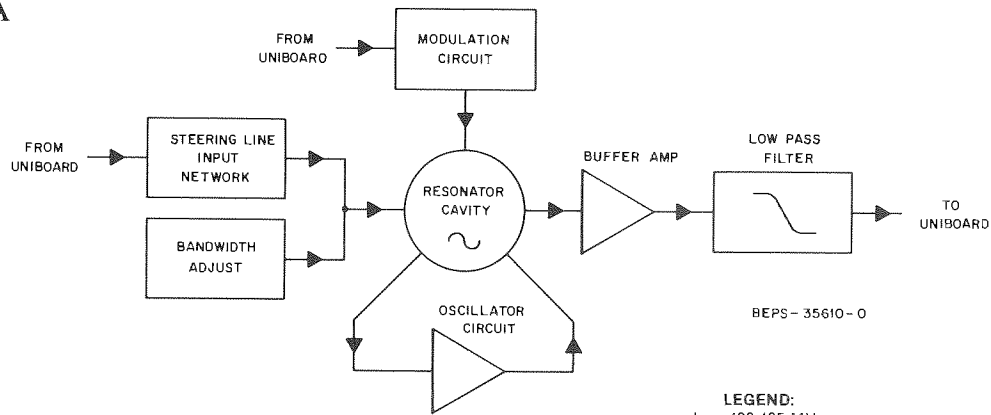
EEPS-35637-0



# SERIES TRANSMIT VCO

## CIRCUIT BOARD DETAIL, BLOCK DIAGRAM, AND PARTS LISTS

### MODEL TTE1470A



**LEGEND:**  
 L = 403-435 MHz  
 M = 435-480 MHz  
 No Code = 403-480 MHz

## parts list

### IMPORTANT

The resonator cavity (Z26) is not repairable. If defective, the entire VCO assembly must be replaced.

### CAUTION

Do NOT remove circuit board from VCO assembly. To do so will destroy proper VCO operation.

TLE5371A Transmit VCO Hardware Kit (403-435 MHz)  
 TLE5372A Transmit VCO Hardware Kit (435-480 MHz) PL-8140-D

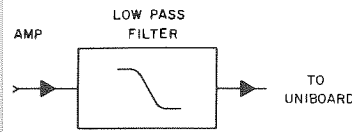
TTE6111A Transmit VCO Board; L  
 TRE6112A Transmit VCO Board; M PL-8139-E

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
A26	1-80752D21	<b>feedthru plate assembly:</b> transmit VCO
J323	9-84135B02	<b>connector, receptacle:</b> phono, female
J324A, 324B	p/o A26	
Z26	not-repairable	<b>resonator cavity:</b> replace entire VCO
<b>non-referenced items</b>		
	2-83718N01	NUT, tension
	3-10932M09	SCREW, tapping; 3 x 0.6 x 6 mm; 5 used
	3-10943M16	SCREW, tapping; 3.5 x 0.6 x 10 mm; 4 used
	3-83100N05	SCREW, tuning (TLE5372A)
	3-83100N10	SCREW, tuning (TLE5271A)
	3-83677N02	SCREW, captive; 4-used
	4-84081N01	WASHER, shoulder; 3-used
	32-82796H02	GASKET, rf mesh
	41-83147N01	SPRING; 4 used
	42-83517N01	RETAINER, spring; 4-used
	15-83190N01	HOUSING; VCO resonator
	15-83191N01	CASTING; VCO resonator

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
C26	21-11035B21	capacitor, fixed: pF ± 5%; 50 V; unless otherwise stated
C27	21-11059B05	100
C28	21-11035B21	.01 uF; ± 20%
C29	21-11035B12	39
C30	21-11035B21	100
C31L	21-11035B16	10
C31M	21-11035B29	7.5
C32 thru 37	21-11035B21	100
C38	21-11035B19	4.7 ± 0.25 pF
C39	21-11035B15	12
C40	21-11035B19	4.7 ± 0.25 pF
C41, 42	21-11035B21	100
C43	21-11078A21	4.7 ± 0.25 pF
C44	21-11031A01	1
CR26	48-84616A01	<b>diode: (see note)</b> silicon, hot carrier
CR27, 28	48-82190H60	silicon, varactor
CR29 thru 34	48-82190H59	silicon, varactor
L26, 27, 28	24-82723H40	<b>coil, rf: nH:</b> unless otherwise stated
L29	24-82723H41	290
L30	24-82723H40	140
L31L	24-84331M03	290
L31M	24-84331M26	5-turns
L32, 33, 34	24-82723H40	8-turns
L35L	24-84331M03	290
L35M	24-84331M04	5-turns
L36L	24-84331M03	4-turns
L36M, 37	24-84331M02	5-turns
L38 thru 41	24-82723H40	290
L42	24-82723H40	290
L43, 44L	76-83960B01	ferrite bead
P324B	9-83730M04	<b>connector, plug:</b> 4-contact; female
Q26	48-869839	<b>transistor: (see note)</b> FET, N-channel; type M9839
Q27	48-84411L83	NPN; type M1183
R26	6-11024A97	<b>resistor, fixed: ± 5% 1/8 W:</b> unless otherwise stated
R27	6-11024A29	100k
R28	6-11024A73	150
R29	6-11024A55	10k
R30L	6-11024A51	1.8k
R30M	6-11024A63	1.2k
R31	6-11024A59	3.9k
R32	6-11024A35	2.7k
R33L	6-11041C67	270
R33M, 34	6-11024A49	1.2k
R35L	6-11024A13	1k
RT26	6-82990E22	33
		<b>thermistor:</b> 190 ohms @ 25C

note: For optimum performance, diodes, transistors, and integrated circuits must be ordered by Motorola part numbers.

# TTE1471A TRANSMIT VCO (403-435 MHz)



BEPS-35610-0

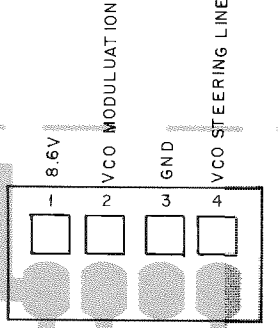
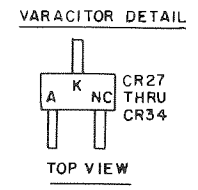
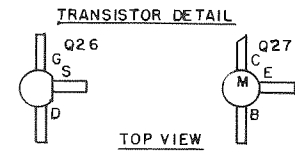
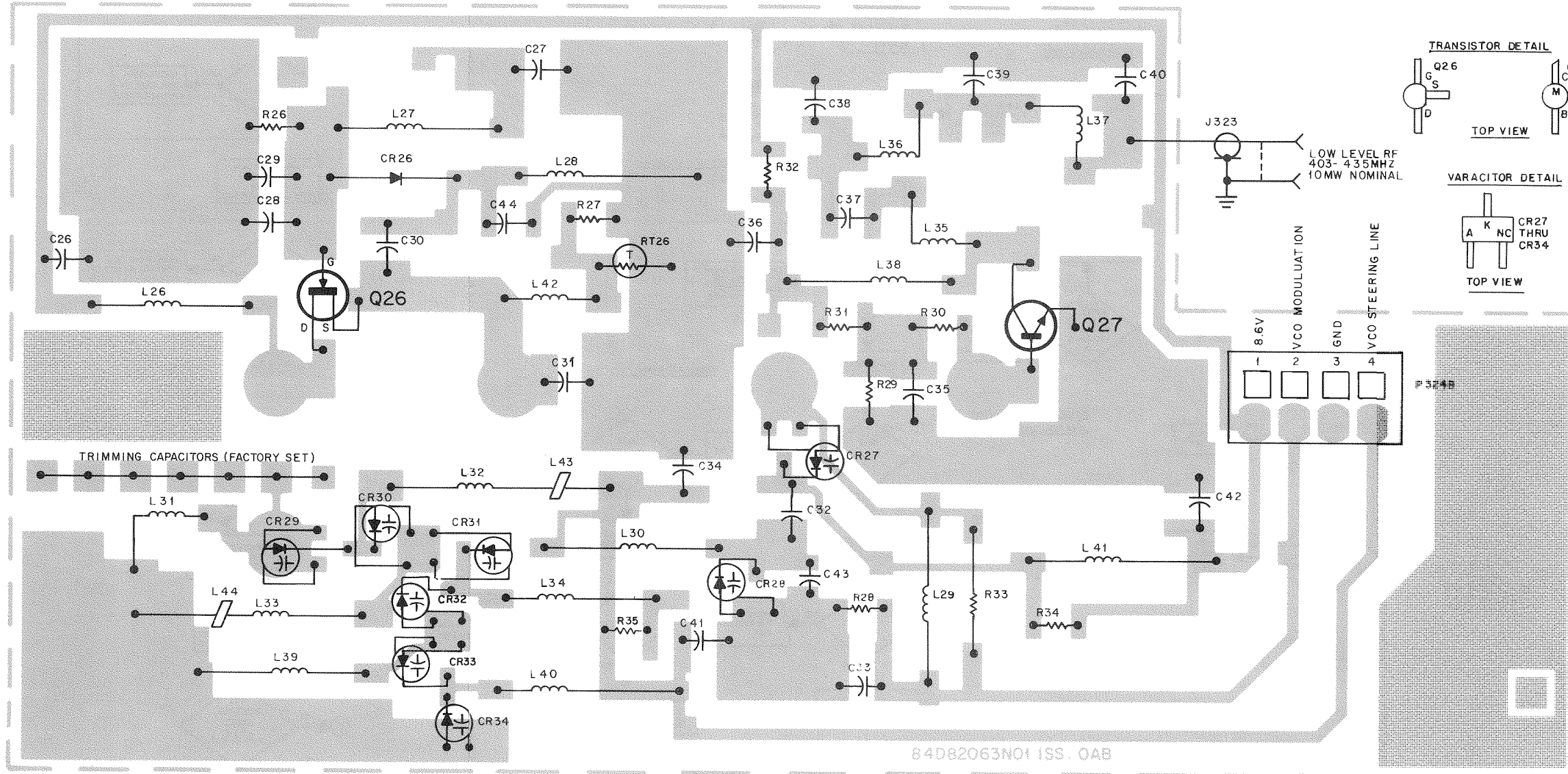
**LEGEND:**  
 L = 403-435 MHz  
 M = 435-480 MHz  
 No Code = 403-480 MHz

**CAUTION**  
 Circuit board from VCO assembly. To do so will  
 CO operation.

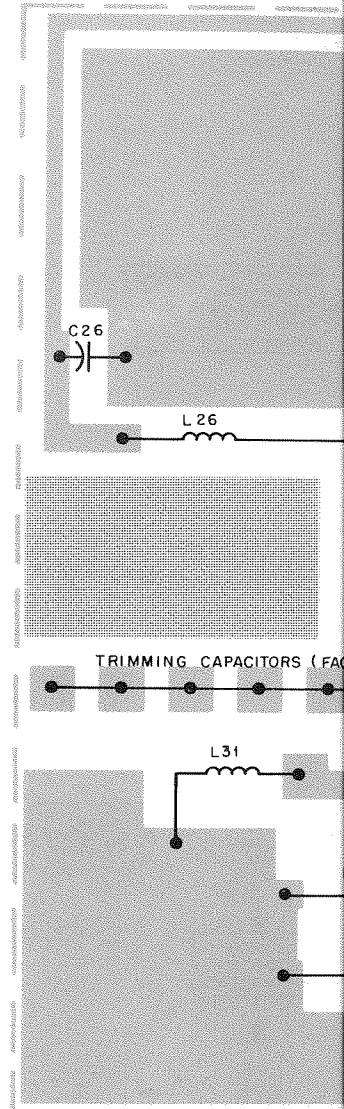
ard; L  
 oard; M  
 PL-8139-E

**TOROLA**  
**RT NO.**

RT NO.	DESCRIPTION
<b>capacitor, fixed: pF ± 5%; 50 V:</b> unless otherwise stated	
35B21	100
59B05	.01 uF; ± 20%
35B21	100
35B12	39
35B21	100
35B16	10
35B29	7.5
35B21	100
35B19	4.7 ± 0.25 pF
35B15	12
35B19	4.7 ± 0.25 pF
35B21	100
78A21	4.7 ± 0.25 pF
31A01	1
<b>diode: (see note)</b>	
16A01	silicon, hot carrier
30H60	silicon, varactor
30H59	silicon, varactor
<b>coil, rf: nH:</b> unless otherwise stated	
23H40	290
23H41	140
23H40	290
31M03	5-turns
31M26	8-turns
23H40	290
31M03	5-turns
31M04	4-turns
31M03	5-turns
31M02	5-turns
23H40	290
23H40	290
20B01	ferrite bead
<b>connector, plug:</b> 4-contact, female	
<b>transistor: (see note)</b>	
139	FET, N-channel; type M9839
1L83	NPN; type M1183
<b>resistor, fixed: ± 5% 1/8 W:</b> unless otherwise stated	
A97	100k
A29	150
A73	10k
A55	1.8k
A51	1.2k
A63	3.9k
A59	2.7k
A35	270
C67	1.2k
A49	1k
A13	33
<b>thermistor:</b>	
E22	190 ohms @ 25C

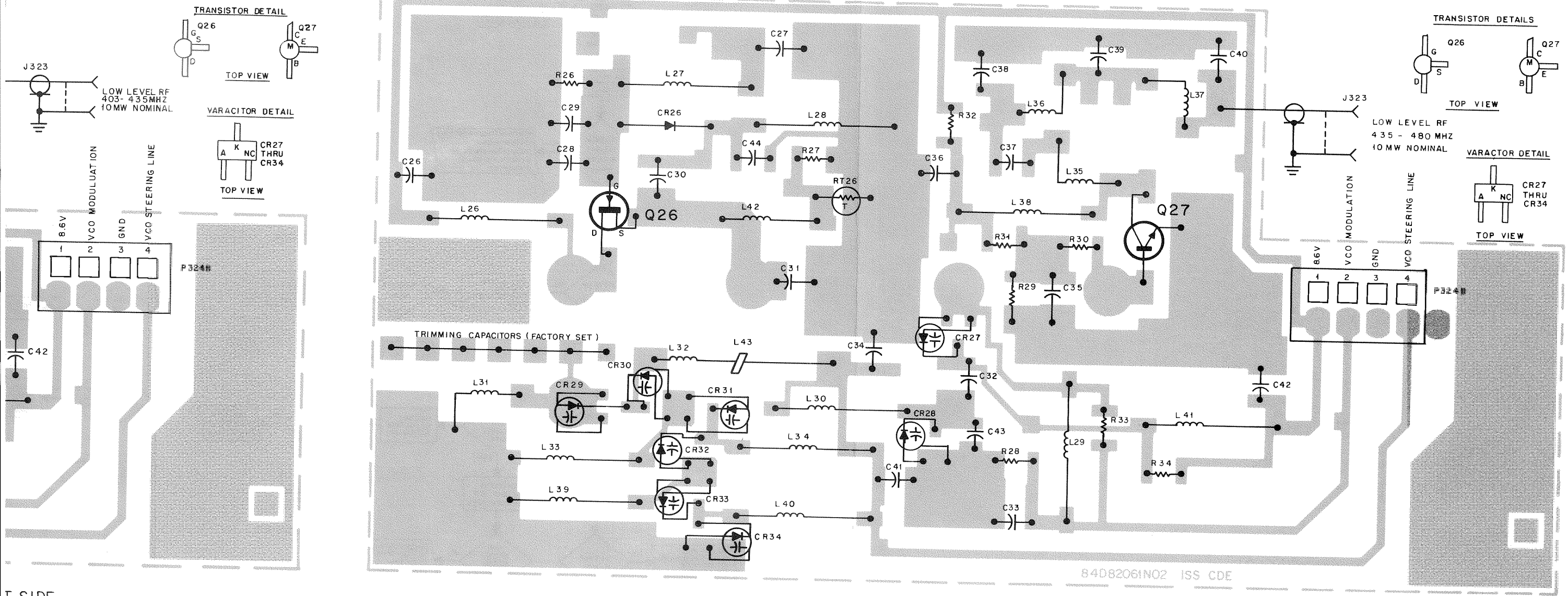


COMPONENT SIDE ● BD-CEPS-40588-0 SHOWN FROM COMPONENT SIDE  
 ○ OL-CEPS-40590-0





# TTE1472A TRANSMIT VCO (435-480 MHz)



T SIDE

COMPONENT SIDE BD-CEPS-35200-A OL-CEPS-35201-C SHOWN FROM COMPONENT SIDE

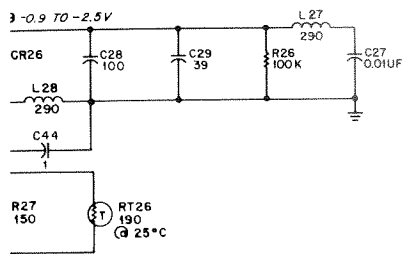
# SERIES TRANSMIT VCO

## SCHEMATIC DIAGRAMS

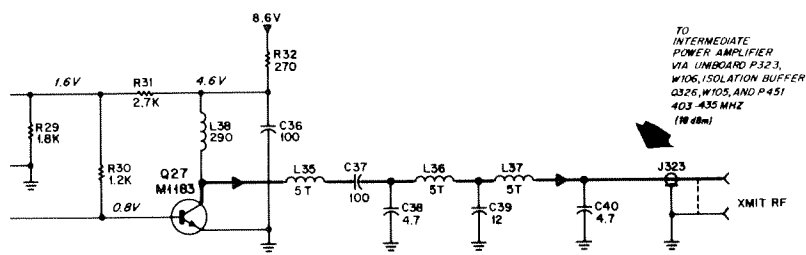
### MODEL TTE1470A

#### TTE1472A TRANSMIT VCO (435-475 MHz)

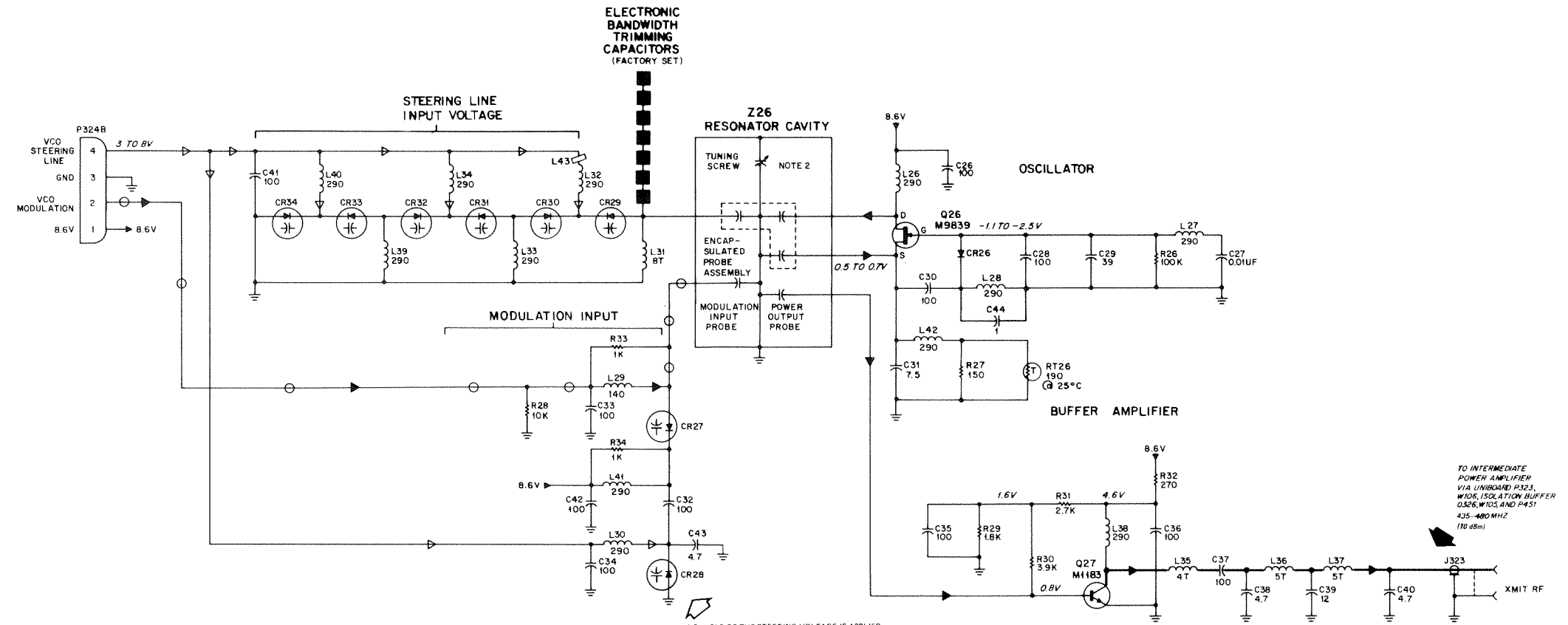
#### OSCILLATOR



#### BUFFER AMPLIFIER



TO INTERMEDIATE POWER AMPLIFIER VIA UNBOARDED P323, W106, ISOLATION BUFFER Q326, W105, AND P451 403-435 MHz (10 dBm)



ELECTRONIC BANDWIDTH TRIMMING CAPACITORS (FACTORY SET)

STEERING LINE INPUT VOLTAGE

Z26 RESONATOR CAVITY

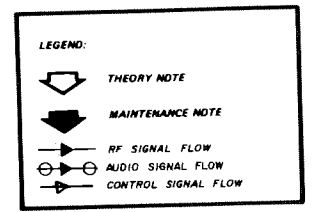
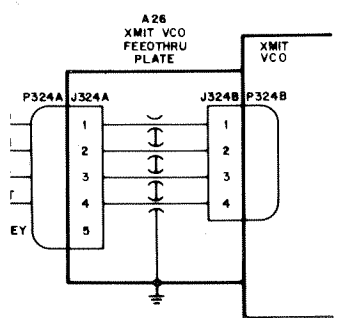
OSCILLATOR

BUFFER AMPLIFIER

A SAMPLE OF THE STEERING VOLTAGE IS APPLIED TO CR28 TO MAINTAIN MODULATION SENSITIVITY OVER THE STEERING LINE VOLTAGE RANGE.

TO INTERMEDIATE POWER AMPLIFIER VIA UNBOARDED P323, W106, ISOLATION BUFFER Q326, W105, AND P451 435-480 MHz (10 dBm)

#### CONNECT DETAIL

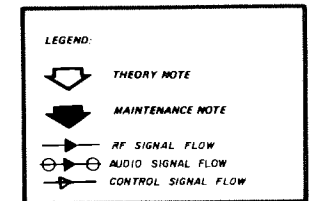
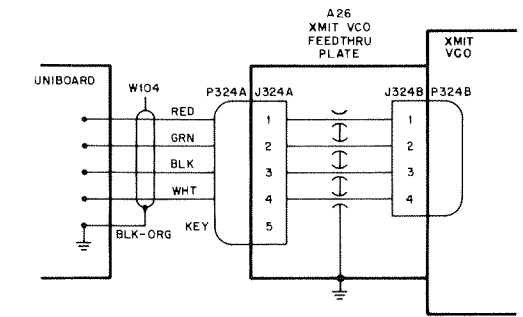


DEPS-40582-A

- NOTES:
- UNLESS OTHERWISE SPECIFIED, ALL RESISTOR VALUES ARE IN OHMS, ALL CAPACITORS IN PICOFARADS, AND ALL INDUCTORS IN NANOHENERIES.
  - THE TUNING SCREW IS FACTORY SET FOR THE PROPER RANGE OF FREQUENCIES.

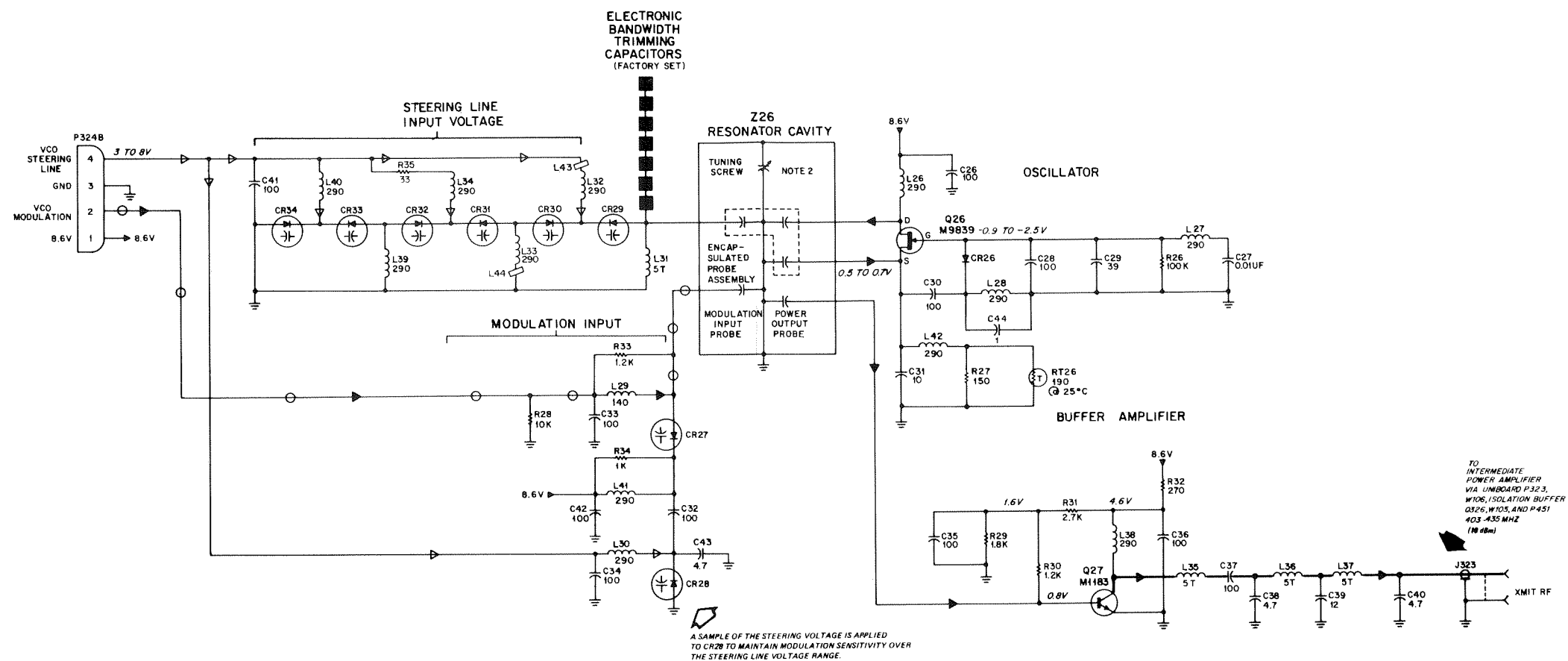
TTE1472A MODEL BREAKDOWN CHART  
 TTE1472A TRANSMIT VCO HARDWARE KIT  
 TTE1472A TRANSMIT VCO BOARD

#### INTERCONNECT DETAIL



DEPS-35083-C

# TTE1471A TRANSMIT VCO (403-435 MHz)



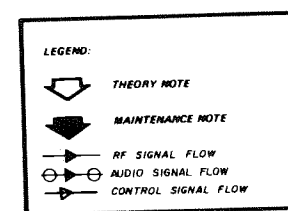
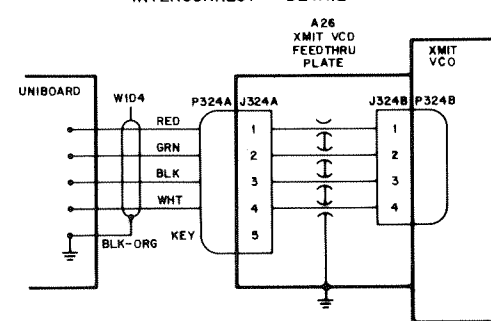
**NOTES:**

1. Unless otherwise specified, all resistor values are in ohms, all capacitors in picofarads, and all inductors in nanohenries.
2. The tuning screw is factory set for the proper range of frequencies.

TTE1471A Model Breakdown Chart

TLE5371A	VCO Hardware Kit
TTE6111A	VCO Board

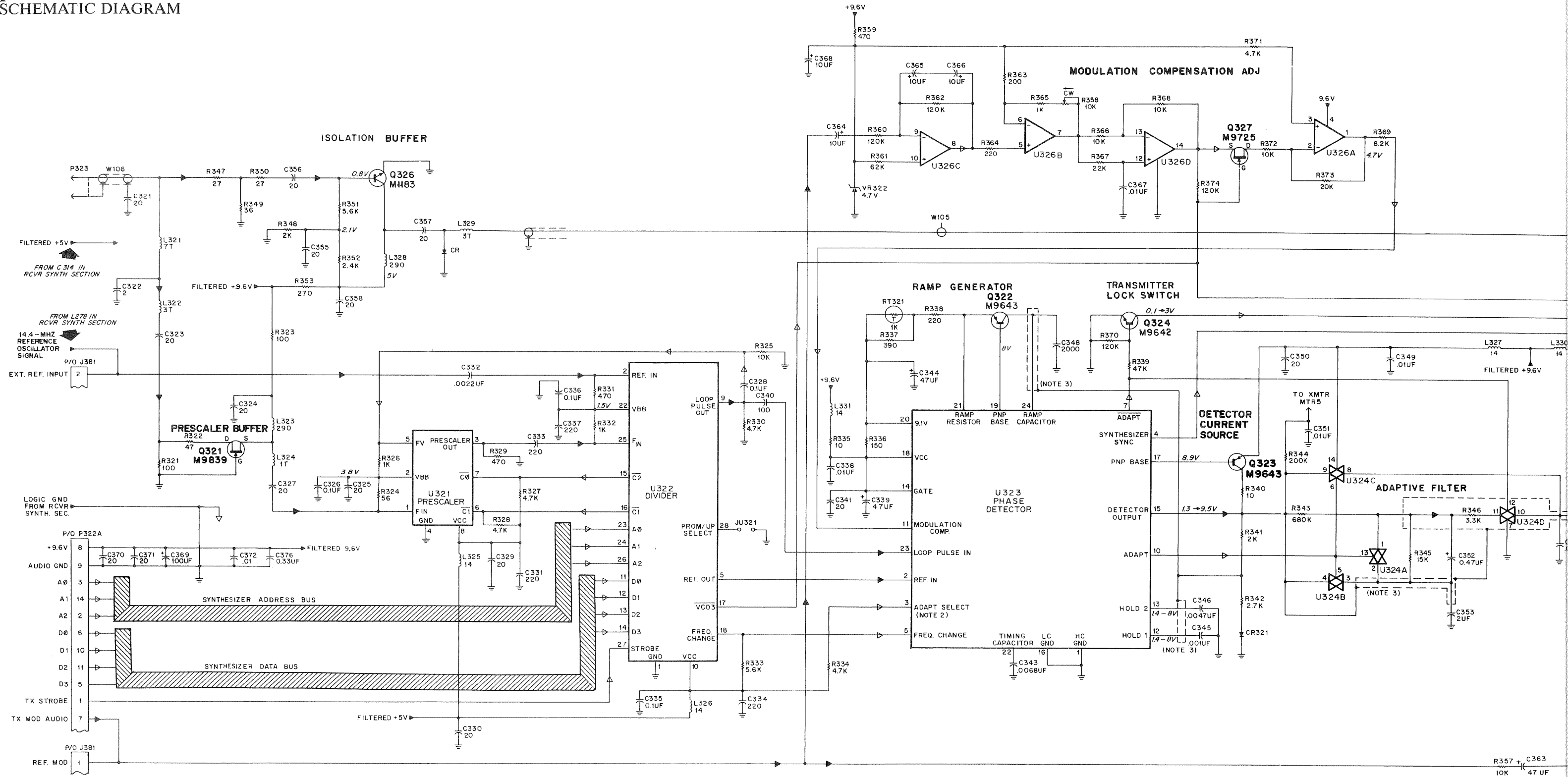
**INTERCONNECT DETAIL**



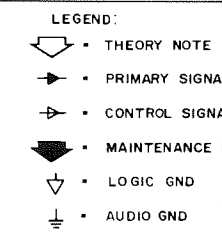
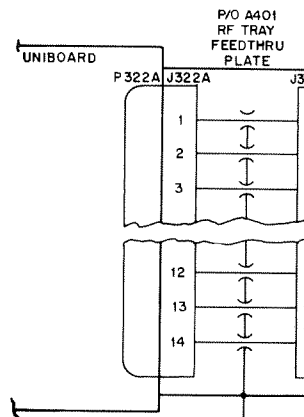
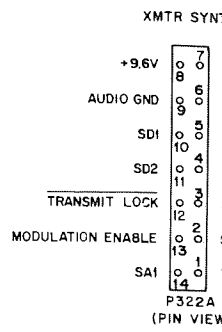
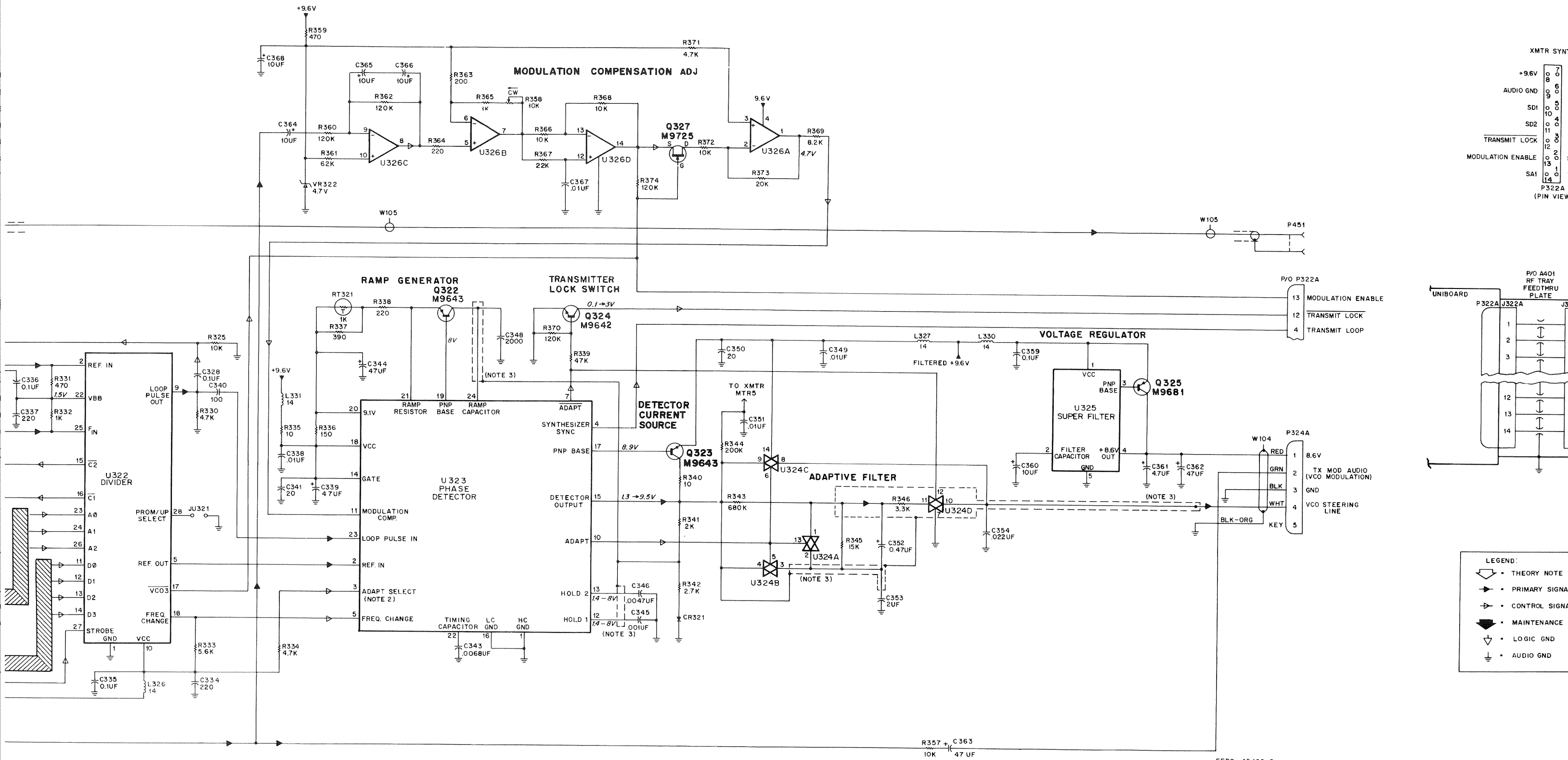
# TRANSMIT SYNTHESIZER

## p/o TRN9880A UNIBOARD

### SCHEMATIC DIAGRAM

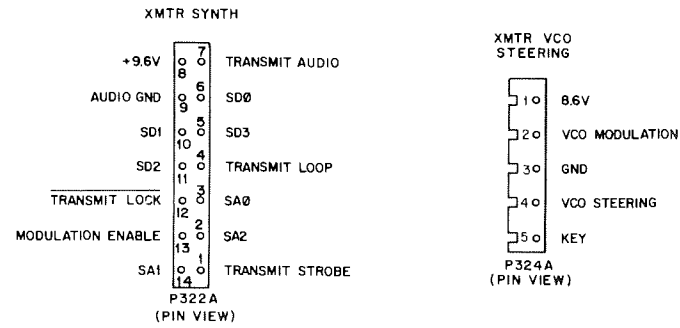


SEE RF TRAY SECTION FOR  
CIRCUIT BOARD DETAIL AND PARTS LIST



R357 + C363  
10K 47UF

### CONNECTOR DETAILS

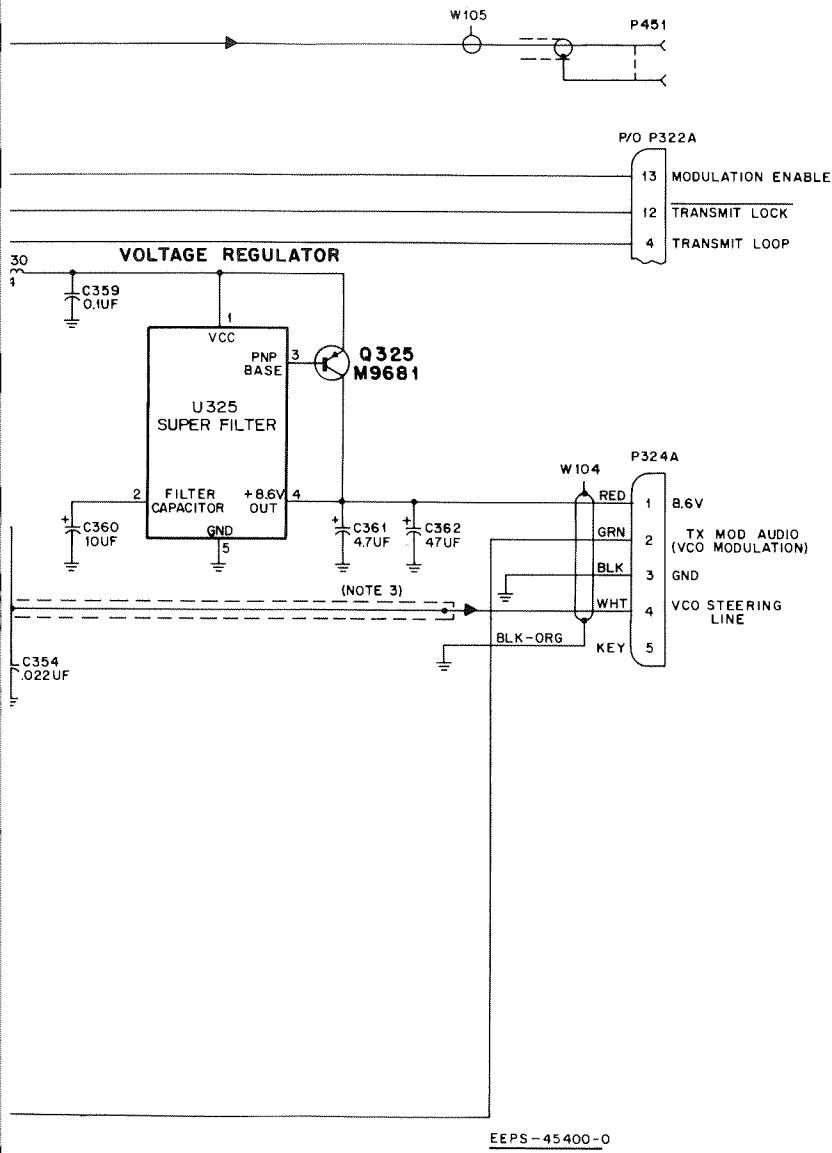
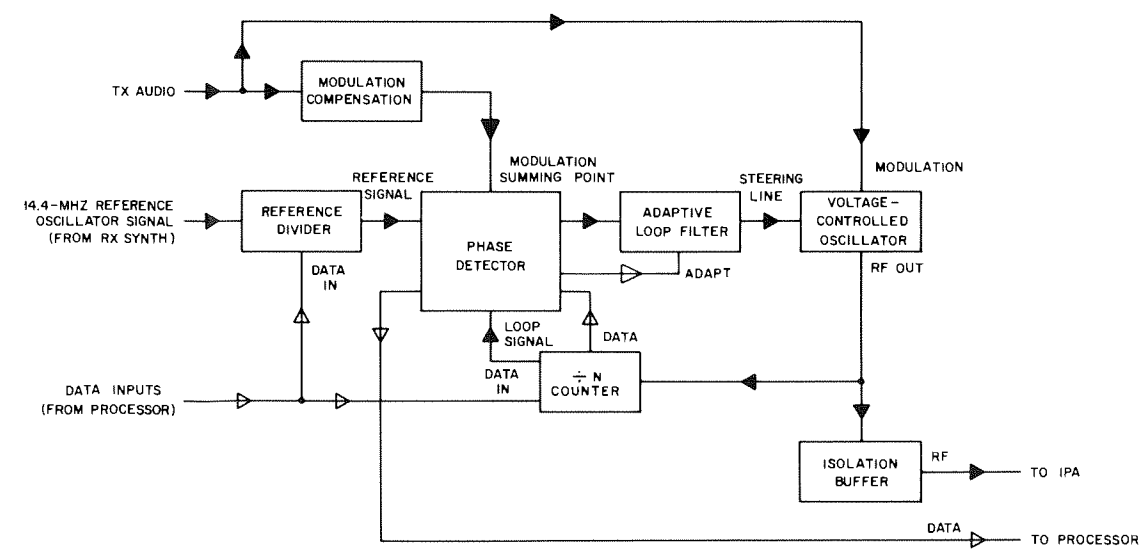
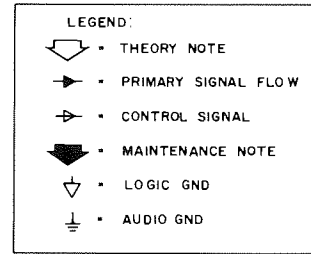
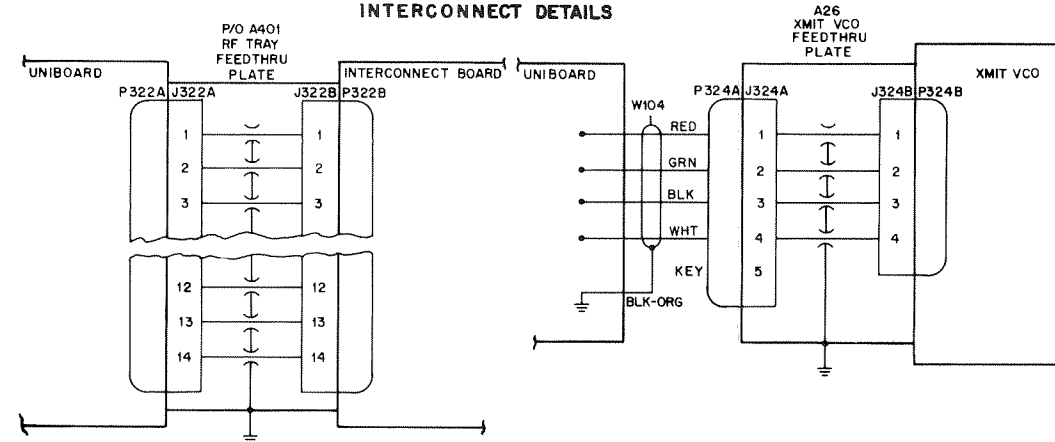


**Notes:**

1. Unless otherwise specified, all resistor values are in ohms, all capacitor values in picofarads, and all inductor values are in microhenries.
2. Long Adapt Signal Period (Slow Lock) is 12 ms.
3. Copper guard bands connected to phase detector U323 output circuit (denoted by dashed lines) surround pins 12, 13, and 24, as well as portions of adaptive filter U324 and the steering line

Ref. Desig.	+ 5 V (Pin)	+ 9.6 V (Pin)	Gnd (Pin)	IC Type Description
U321	8	—	4	Prescaler
U322	10	—	1	Divider
U323	—	18, 14	1, 16	Phase Detector
U324	—	14	7	Analog Gate
U325	—	1	5	Super Filter
U326	—	4	11	Quad Op. Amplifier

### INTERCONNECT DETAILS



EEPS-45400-0

BEPS-35604-0



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## 1. IPA THEORY OF OPERATION

1.1 The *MSF 5000* IPA consists of four cascaded amplifier stages. The four stages are incorporated onto a single ceramic substrate using micro-strip line design. The IPA input and output impedance is 50 ohms.

1.2 The rf output generated by the XMIT VCO (at least 10 mW), at the required transmit frequency, is applied to the first stage of the IPA (Q459), a class A amplifier with a fixed supply voltage, A + . The remaining three amplifiers operate with a variable control voltage. The power output from the IPA depends upon the level of control voltage. Therefore, the power output of the radio can be smoothly varied by changing the IPA control voltage. DC power for the IPA is routed from the uniboard through cable W701 to P452. The IPA module has a rated power output of 0 to 9 watts.

1.3 Since the transmit VCO operates whether the radio is in the transmit mode or receive mode, it is possible for rf energy at the transmit frequency to be conducted through the IPA to the antenna even when the radio is operating as a receiver. An IPA attenuation circuit reduces this undesirable signal to a very low level by turning the IPA "off" (saturating it) . That is, the attenuation circuit is composed of transistor switches Q453, Q454, and Q455. When in the receive mode, each of these transistors provides a direct current that forward biases the base-emitter junctions of each of the first three IPA amplifier stages. In this saturated condition very little rf energy can be conducted through the amplifiers. Therefore, the VCO transmit signal is effectively reduced during receiver operation. During transmit, the three attenuation transistors are switched off and the IPA amplifier stages operate normally.

## 2. 9.6 V REGULATOR THEORY OF OPERATION

The 9.6 volt output is obtained from a series regulator circuit on the IPA carrier circuit board (TRN5145A). The 9.6 volt regulator uses the A + output from the ferroresonant power supply as a source voltage. A 9.6 volt sensing circuit regulates the amount of current that is

allowed to pass through the series regulator, thus controlling the voltage across the load. Filtering of the 9.6 volt regulator's output is done on the uniboard.

## 3. MAINTENANCE

### 3.1 IPA REMOVAL

The *MSF 5000* IPA assembly can be removed as follows, after removal of the rf tray cover.

Step 1. Disconnect IPA input cable W105 rf connector P451.

Step 2. Disconnect IPA output cable W601 connector P453 from prefilter (p/o FL500 transmitter filtering option) or straight adapter CP451 (standard models). Remove cable restraint(s) holding the IPA output cable W601 to the station chassis.

Step 3. Disconnect IPA dc interconnect cable W701 connector P452.

Step 4. Loosen five captivated IPA mounting screws. The IPA assembly (hybrid + carrier board + heat sink) can now be lifted from the rf tray.

Step 5. Remove IPA assembly handle with a pair of needlenose pliers.

---

### CAUTION

Do not stress the IPA hybrid when removing the IPA handle.

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Step 6. Remove the nuts from the two stud-mounted transistors (Q461 and Q462) with a 1/4" nut driver.

Step 7. Carefully unsolder the two grounding straps and center conductor of IPA output cable W601.

Step 8. Carefully unsolder the four Omega straps connecting the IPA hybrid to the IPA carrier board.

---

**CAUTION**

Excessive heating during the unsoldering operation can cause the microstrip solder lugs to become loose.

---

Step 9. Carefully unsolder the seven wire jumpers from the solder lugs on the IPA hybrid.

Step 10. The IPA hybrid can now be lifted from the IPA printed-circuit board and replaced.

### 3.2 IPA REPLACEMENT

Use the following procedure to replace the IPA ceramic hybrid:

Step 1. All steps relating to the removal of the IPA can be reversed, with particular attention being paid to the following items:

- Wakefield Thermal Compound should be applied as required around the clearance holes in the IPA heat sink for the studded transistors.
- Follow the proper procedure for installing Omega straps, as described in the Maintenance section of this manual.
- Before placing the IPA assembly back into the rf tray, a coating of Wakefield Thermal Compound should be applied to the IPA mounting surface of the rf tray.

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**CAUTION**

Application of a thick coating of thermal compound or the presence of foreign material on the mounting surface may cause poor thermal contact and may result in early transistor failure.

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## 4. IPA TROUBLESHOOTING PROCEDURE

### 4.1 POWER OUTPUT

Refer to the IPA Troubleshooting Chart at the end of this section while performing these procedures. Also, refer to the Station Functional Block Diagram in the Description section of this manual.

Step 1. With station powered up, put station in transmit mode (set S802 to XMIT). Measure IPA power output. Power output should be at least 8 W.

Step 2. If power output is low or zero, check for IPA control voltage at the collectors of Q460, Q461, Q462, and A+ on the collector of Q459.

Step 3. If control voltage is at least 11 volts on all three controlled stages and A+ is available to Q459, check the VCO buffer amplifier gain (greater than 1 dB) and the VCO

output (greater than 7 mW). If the buffer amp or VCO are operating incorrectly, then refer to the Synthesizer Troubleshooting Charts in this manual.

Step 4. If the control voltage is below 11 volts, check Q451 for an open circuit. If Q451 is defective, replace it.

Step 5. Check the IPA attenuation circuit, as follows:

Step 6. If all voltage levels on the amplifier and attenuation circuit are within limits, replace IPA. See IPA removal procedure.

### 4.2 ATTENUATION CIRCUIT

The attenuation circuit can be tested in either the receive mode or the transmit mode. The following steps are applicable to both modes, but with information relating to the transmit mode in parentheses; e.g. (transmit).

Step 1. Make sure station is in the receive (transmit) mode.

Step 2. Measure the voltage at the collector of Q455. Measure the voltage at the emitter of Q453 and Q454. These voltages should be at least 11 volts (approximately 0 volts).

Step 3. If Q455 is less than 11 volts (approximately 0 volts), check P452-2. It should be approximately 0 volts (A+). If P452-2 voltage is OK, replace Q455. If voltage is incorrect, check the power control troubleshooting guide.

Step 4. If Q453 or Q454 is less than 11 volts (approximately 0 volts), check the collector of Q452. It should be A+ volts (approximately 0 volts). If not, replace Q452. If Q452 is at A+ (approximately 0 volts), replace either Q453 or Q454 as required.

## 5. 9.6 V REGULATOR TROUBLESHOOTING PROCEDURE

Step 1. Check that A+ is available at the emitter of Q456.

Step 2. Check that the regulator output is not shorted. Regulator output is shorted if CR453 is forward biased. If the regulator is shorted, investigate and repair.

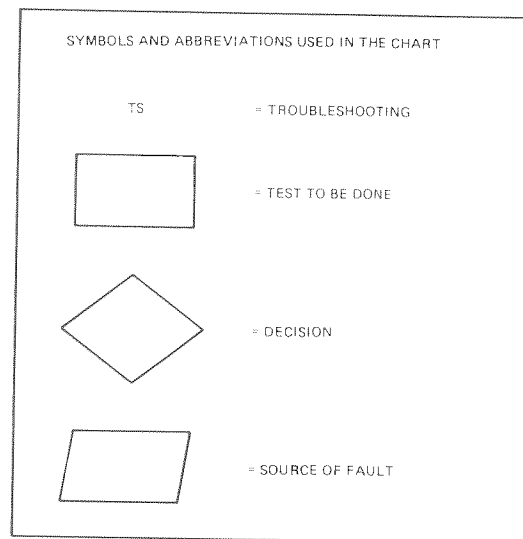
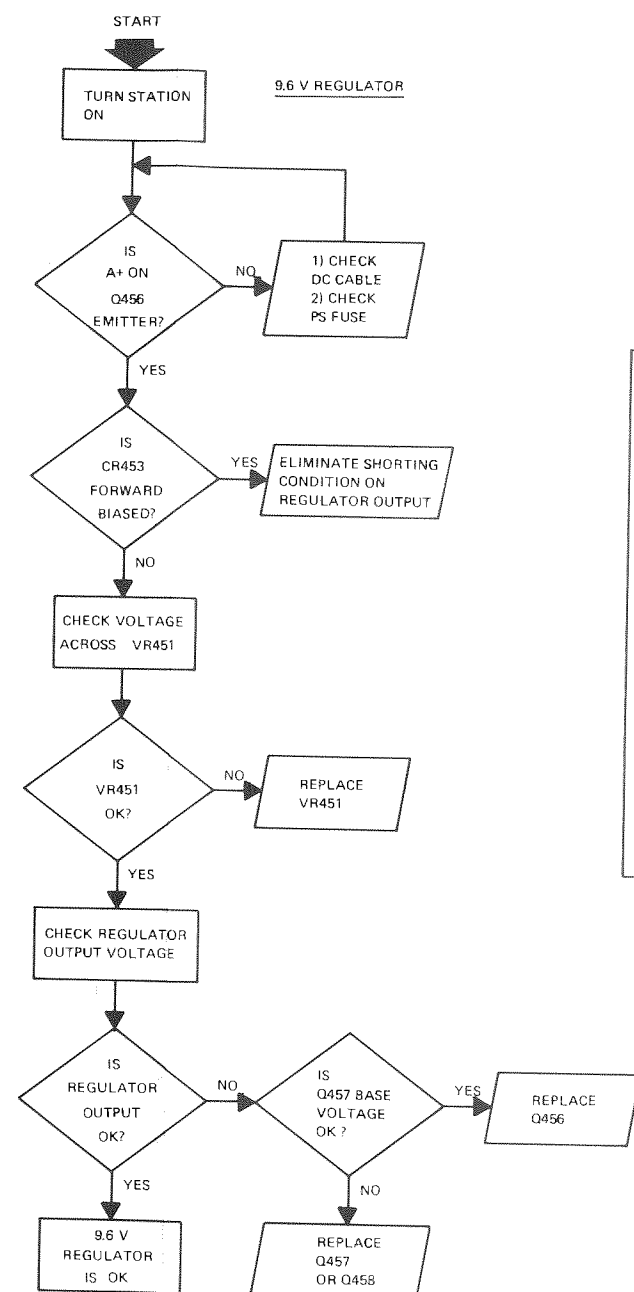
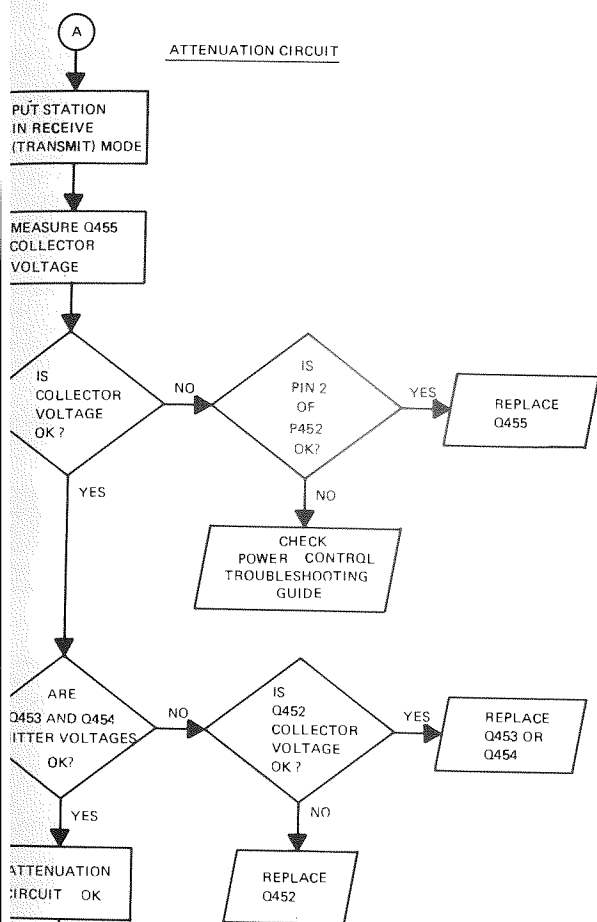
Step 3. Check the voltage across VR451. If regulator output is above 9 volts, the voltage across VR451 should be approximately 8.2 volts. If regulator voltage is below 9 volts, the regulator output and diode voltage should be identical. If not, replace VR451.

Step 4. If the voltage is above 10.5 volts, check the voltage on the base of Q457. It should be under 4 volts. If it is under 4 volts, replace Q456. If it is under 4 volts, replace Q456. If it above 4 volts, replace Q458 or Q457.

Step 5. If the output voltage is too low (less than 8.5 volts), check the voltage on base of Q457. It should be above 4 volts. If it is above 4 volts, replace Q458 or Q457.



# IPA AND 9.6 V REGULATOR TROUBLESHOOTING CHART



**TROUBLESHOOTING PREREQUISITES**

STEP 1. INSTALL STATION CONTROL BOARD SERVICE JUMPER (JU1) ONTO ITS SERVICE INSTALLATION POSITION.

IMPORTANT  
WHEN TROUBLESHOOTING IS COMPLETED, RETURN JU1 TO ITS ORIGINAL POSITION.

STEP 2. DISCONNECT THE IPA OUTPUT CABLE (W601) BY UNSCREWING P453 FROM THE STRAIGHT ADAPTER CP451.

STEP 3. CONNECT W601 (VIA P453) TO A WATTMETER TERMINATED IN A 50-OHM LOAD. BE SURE THE WATTMETER AND LOAD ARE RATED FOR USE AT UHF.

DEPS-35642-0

**MODEL COMPLEMENT**

MODEL		DESCRIPTION
	p/o TUE1761A	RF Tray; 403-435 MHz
	p/o TUE1762A	RF Tray; 435-475 MHz
	p/o TUE1901A	RF Tray (T/R = 3-20 MHz); 403-435 MHz

**LEGEND:**  
X = one item supplied

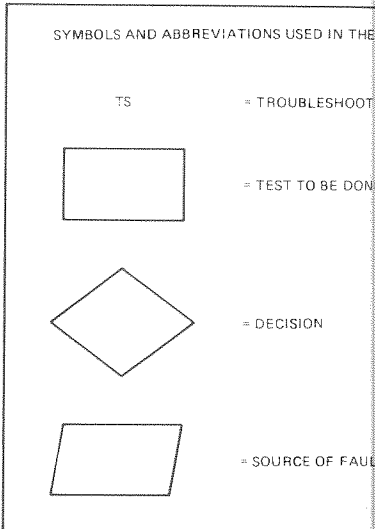
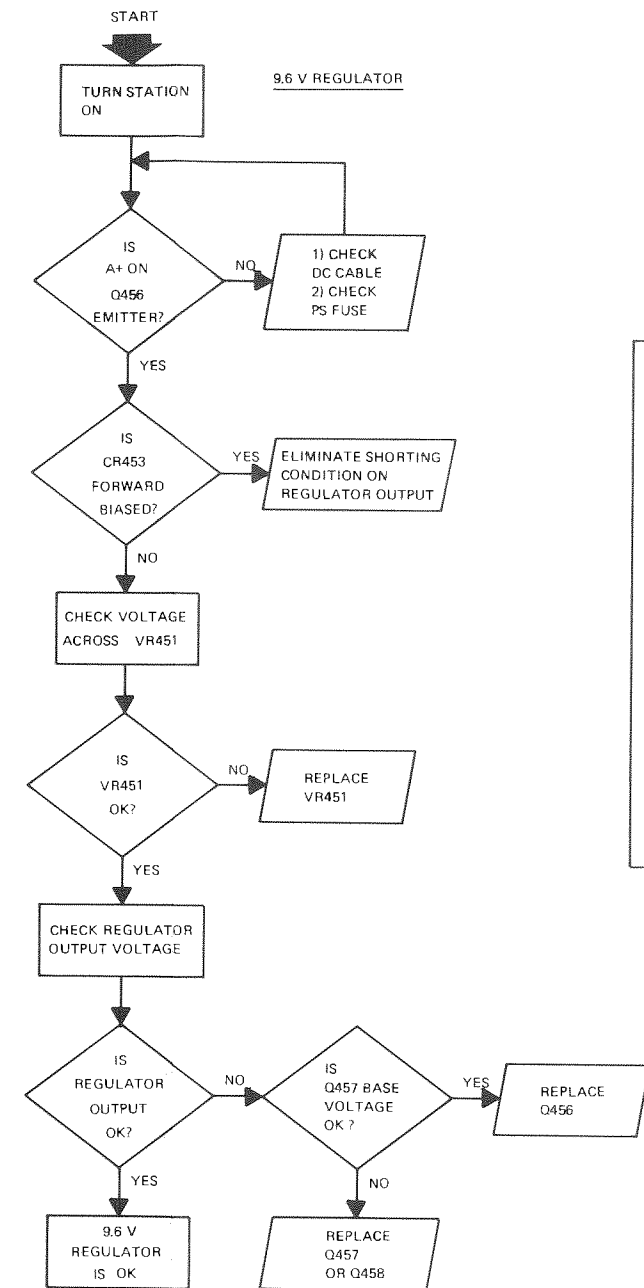
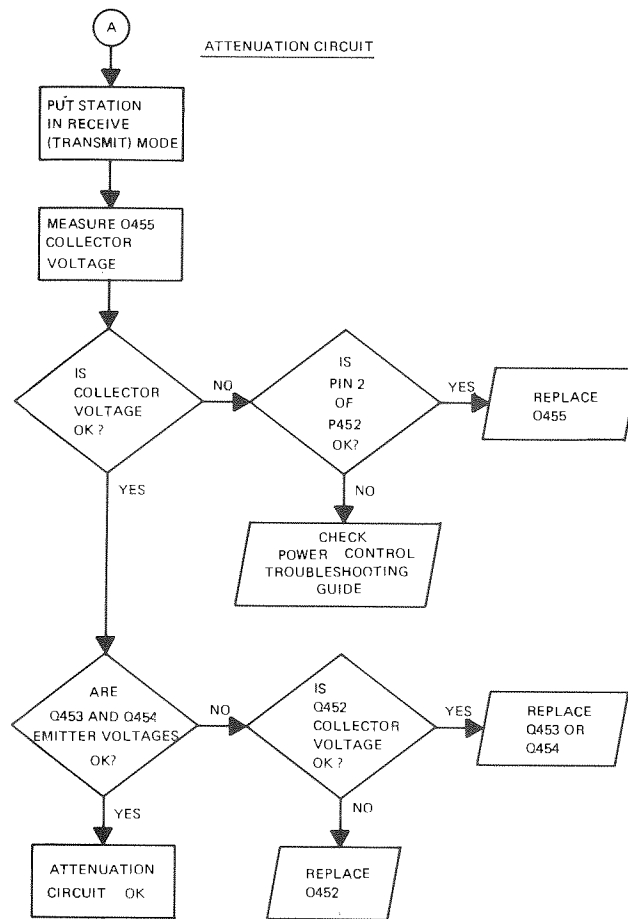
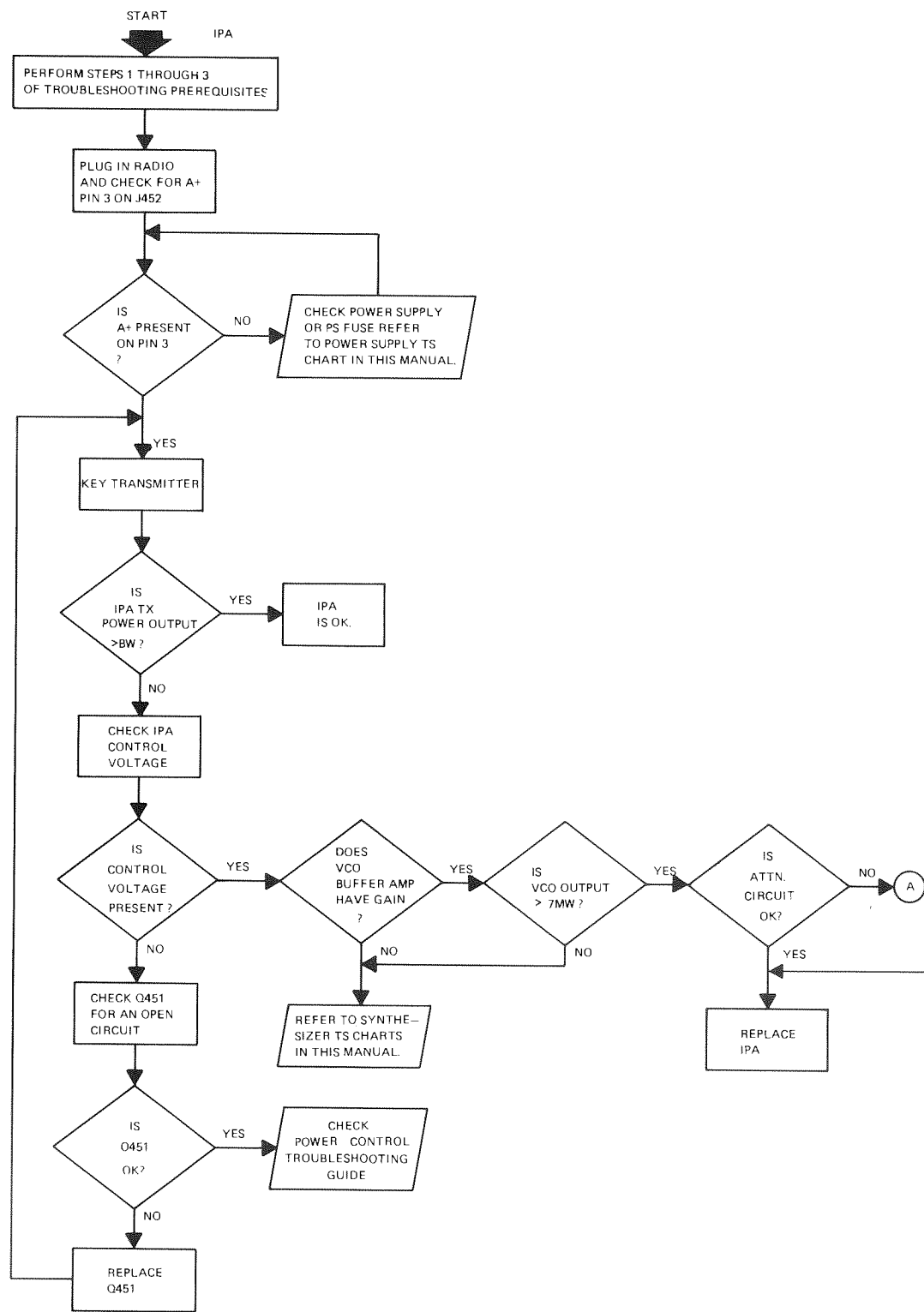
KIT		DESCRIPTION
X	TFE6481A	Injection/Image Filters; 403-435 MHz
	TFE6482A	Injection/Image Filters; 435-475 MHz
X	TLE5321A	Injection/Amplifier Board; 403-435 MHz
	TLE5322A	Injection/Amplifier Board; 435-475 MHz
X	TLE5391A	Preselector; 403-435 MHz
	TLE5392A	Preselector; 435-475 MHz
X	TLE5401A	Front End; 403-435 MHz
	TLE5402A/B	Front End; 435-475 MHz
	X TLE5701A	Front End (T/R = 3-20 MHz); 403-435 MHz
	X TLE5711A	Preselector (T/R = 3-20 MHz); 403-435 MHz

**MODEL COMPLEMENT BREAKDOWN**

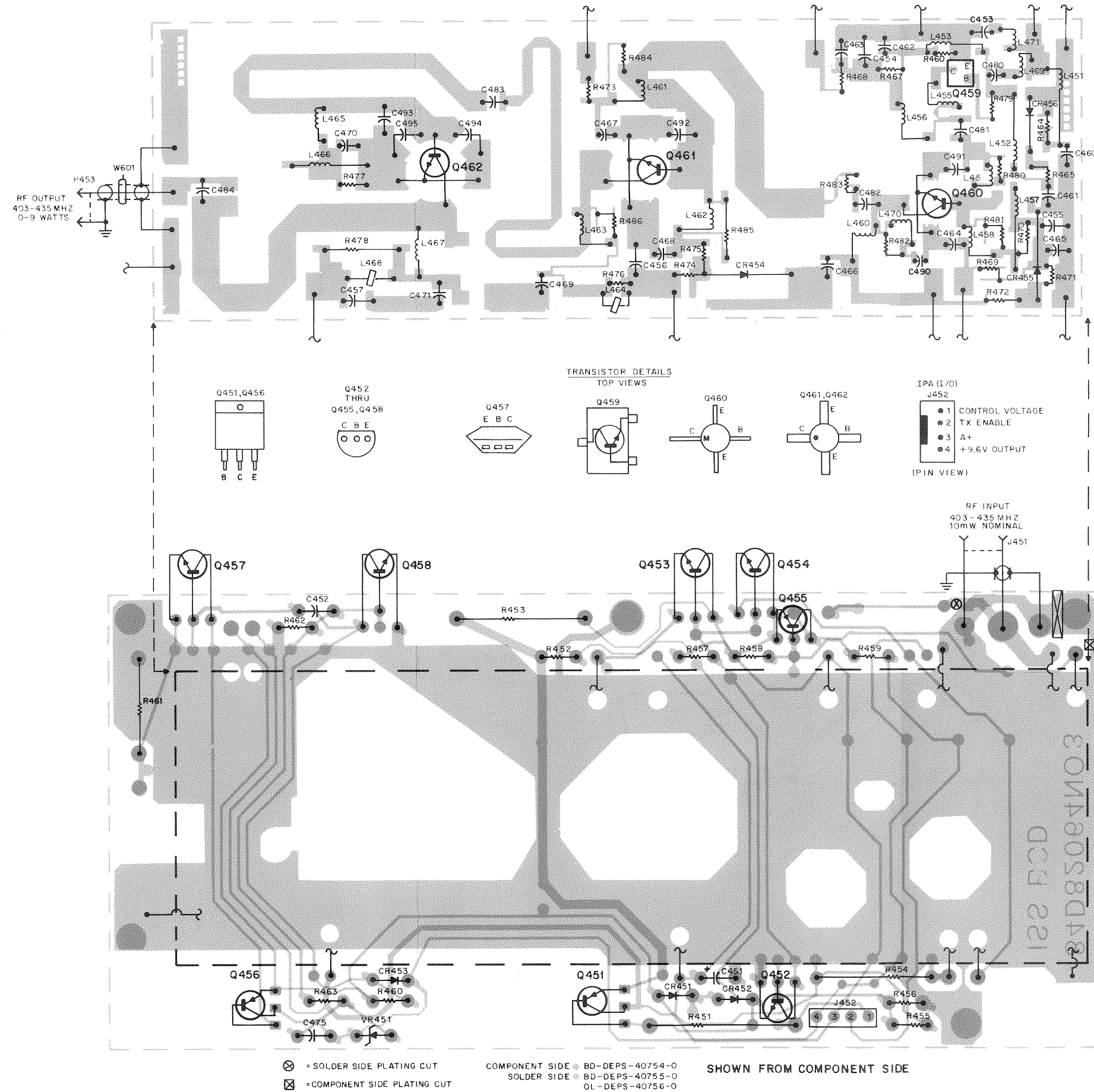
MODEL		DESCRIPTION
	TLE2231A	Intermediate Power Amplifier; 403-435 MHz
	TLE2232A	Intermediate Power Amplifier; 435-475 MHz

**LEGEND:**  
X = one item supplied

KIT		DESCRIPTION
X	X	TKN8843A IPA Output Cable Kit
X		TLE5331A IPA Hybrid Circuit Kit (403-435 MHz)
	X	TLE5332A IPA Hybrid Circuit Kit (435-475 MHz)
	X	TRN5145A IPA Carrier Board Kit (435-475 MHz)
X	X	TRN5146A IPA Hardware Kit
X		TRN9667A IPA Carrier Board Kit (435-475 MHz)



**IPA AND 9.6 V  
REGULATOR (403-435 MHz)  
CIRCUIT BOARD DETAIL AND PARTS LISTS**



**parts list**

Field repair of these replaced in their en-  
reference purposes of  
TRN5145A IPA Carrier Board  
TRN9667A IPA Carrier Board

REFERENCE NUMBER	MOTOR PART
C451	23-84538
C452	8-11017B
C453 thru 473	not p/o k
C474M	21-85129
C475	21-11014
CR451,452	48-82466
CR453	48-11034
CR454	not p/o k
CR455M	48-11034
CR456M	48-83654
J452	28-83143
J451	9-84231B
Q451	48-86980
Q452,453,454	48-86964
Q455	48-86964
Q456	48-86980
Q457	48-86964
Q458	48-86964
R451	17-82291
R452	6-11009E
R453L	17-82039
R453M	17-82291
R454L	6-11045A
R454M	17-82291
R455	6-11009E
R456	6-11009E
R457	6-11009E
R458	6-11009E
R459,460	6-11009E
R461	6-126C29
R462,463	6-10621A
R464M	6-11009E
VR451	48-83461
TRN5146A IPA Hardware Kit	
2-7007	
2-8364	
3-83677N	
3-83678N	
4-7691	
4-82345A	
10-10043	
14-83820	
42-83680	
54-84697	
55-83679	
64-83132	
75-10605	
TKN8842A IPA Feedthru Cable	
P452	15-83142
P454B	15-84301
39-82717	
42-10217	
TKN8843A Coaxial Cable with	
P453	28-84474
30-84174	
33-8808	
43-8315	

# parts list

**LEGEND:**  
 L = 403-435 MHz  
 M = 435-475 MHz  
 No Code = 403-475 MHz

**LEGEND:**  
 L = 403-435 MHz  
 M = 435-475 MHz  
 No Code = 403-475 MHz

**IMPORTANT**

Field repair of these kits is not recommended. They should be replaced in their entirety. The following parts are listed for reference purposes only.

TRN5145A IPA Carrier Board Kit; M  
 TRN9667A IPA Carrier Board Kit; L PL-8132-C

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
C451	23-84538G23	capacitor, fixed: 15 uF ± 20%; 20 V
C452	8-11017B11	.022 uF ± 5%; 50 V
C453 thru 473		not p/o kits
C474M	21-851299	600 pF ± 10%; 600 V
C475	21-11014H32	20 pF ± 5%; 100 V
CR451,452	48-82466H18	diode: (see note) silicon
CR453	48-11034D01	silicon
CR454		not p/o kits
CR455M	48-11034D01	silicon
CR456M	48-83654H01	silicon
J452	28-83143M05	connector: male, 4 contact
J451	9-84231B02	female, single contact
Q451	48-869807	transistor: (see note) PNP; type M9807
Q452,453,454	48-869642	NPN; type M9642
Q455	48-869643	PNP; type M9643
Q456	48-869807	PNP; type M9807
Q457	48-869640	NPN; type M9640
Q458	48-869642	NPN; type M9642
R451	17-82291B21	resistor, fixed; ± 5% 1/4 W; unless otherwise stated 100; 3 W
R452	6-11009E41	470
R453L	17-82036G24	0.13 ± 5%; 2 W
R453M	17-82291B29	0.20 ± 1%; 2 W
R454L	6-11045A12	30; 1/2 W
R454M	17-82291B43	82 ± 10%; 3 W
R455	6-11009E57	2.2k
R456	6-11009E65	4.7k
R457	6-11009E57	2.2k
R458	6-11009E73	10k
R459,460	6-11009E57	2.2k
R461	6-126C29	150 ± 10%; 1 W
R462,463	6-10621A60	41.2 ± 1%; 1/8 W
R464M	6-11009E49	1k
VR451	48-83461E32	voltage, regulator: Zener; 8.2 V

TRN5146A IPA Hardware Kit PL-8131-C

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
non-referenced items		
	2-7007	NUT, hex 8-32 x 1/4 x 3/32"; 2-used
	2-8364	NUT, hex 3/8-32 x 1/2 x 3/32"
	3-83677N02	SCREW, captive; 5-used
	3-83678N03	SCREW, tapping; 2-used
	4-7691	WASHER, lock; 3/8"; internal
	4-82345A18	WASHER, shoulder; 2-used
	10-10043A02	STRAP, tie-wrap; 6-used
	14-83820M02	INSULATOR, thermoconductive; 2-used
	42-83680N04	STRAP, omega; 4 used
	54-84697B01	LABEL
	55-83679N01	HANDLE
	64-83132N01	PLATE, heatsink
	75-10605A04	CUSHION, plastic foam; 12"-used

TKN8842A IPA Feedthru Cable PL-8251-A

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
P452	15-83142M05	connector, receptacle: housing, 4-position
P454B	15-84301K02	housing, 4-position
non-referenced items		
	39-82717M01	CONTACT, receptacle; 8-used
	42-10217A02	STRAP, tie-wrap; 2-used

TKN8843A Coaxial Cable with Connector PL-8277-A

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
P453	28-84476G01	connector, plug: male, single contact
non-referenced items		
	30-84173E01	CABLE, coaxial; double shield; 36"-used
	33-88083C06	DECAL, color strip; BLU
	43-83152N02	BUSHING, cable

**IMPORTANT**

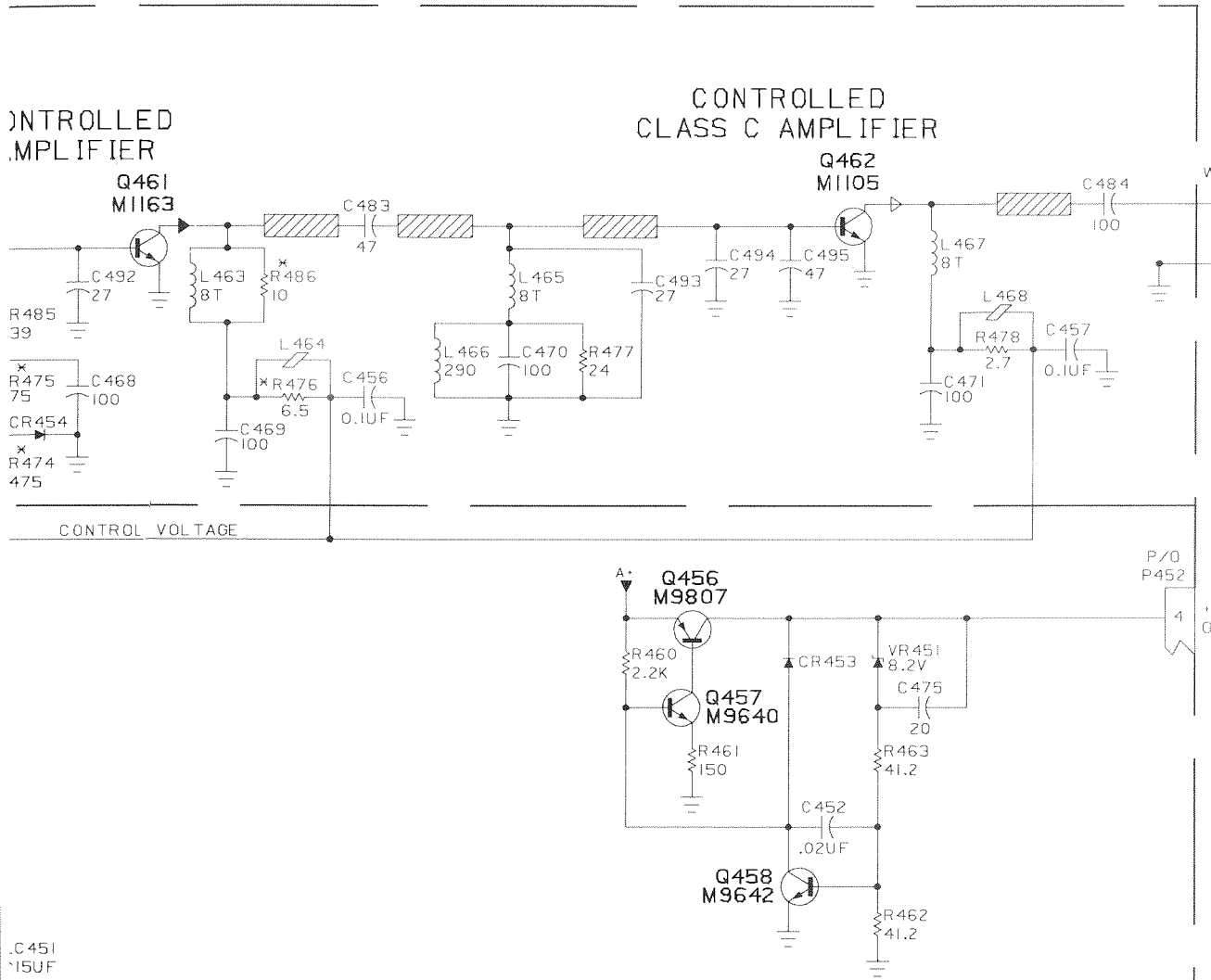
Field repair of these kits is not recommended. They should be replaced in their entirety. The following parts are listed for reference purposes only.

TLE5331A IPA Hybrid Circuit; L  
 TLE5332A IPA Hybrid Circuit; M PL-8130-C

REFERENCE NUMBER	MOTOROLA PART NO.	DESCRIPTION
C453L	21-11059D59	capacitor, fixed: pF ± 5% 50 V; unless otherwise stated 100
C453M,454,455L	21-11059B13	0.1 uF ± 10%
C456,457,458M	21-11059B13	0.1 uF ± 10%
C459M	21-11059D60	2.7 ± 0.25 pF
C460 thru 470	21-11059D59	100
C471L	21-11059D59	100
C471M	21-11078827	30
C472M,473M	21-11078B34	47
C474 thru 479		not p/o kits
C480L	21-11059D59	100
C481L,482L	21-11059C21	100
C483L	21-11078B34	47
C484L	21-11059C21	100
C485 thru 489		not p/o kits
C490L	21-11059D59	100
C491L	21-11078B19	16
C492L,493L,494L	21-11078B25	27
C495L	21-11078B34	47
CR454,455L	48-82392B05	diode: (see note) silicon
CR456L	48-83654H01	silicon
L451L	24-82723H40	coil, rf: 290 nH; YEL-BLK
L451M	1-80702T04	assembly, wire and bead includes: BEAD, ferrite
L452L	24-82723H40	290 nH; YEL-BLK
L452M	24-80202B01	assembly; choke; 3-turns and bead
L453L	24-82723H40	290 nH; YEL-BLK
L454		not p/o kits
L455L	24-83035N27	8-turns
L456L	24-84331M25	8-turns
L457L	24-82723H40	290 nH; YEL-BLK
L458L	24-84331M25	8-turns
L459L	24-83035N12	3-turns
L460L thru 463L	24-84331M25	8-turns
L464L	1-80702T04	assembly, wire and bead includes: BEAD, ferrite
L465L	24-84331M25	8-turns
L466L	24-82723H40	290 nH; YEL-BLK
L467L	24-84331M25	8-turns
L468M	1-80702T04	assembly, wire and bead includes: BEAD, ferrite
L469L	24-83035N12	3-turns
L470L	24-83035N27	8-turns
L471L	24-83035N09	7-turns
Q459	48-84939C31	transistor: (see note) NPN; type M3931
Q460	48-84411L37	NPN; type M1137
Q461	48-84411L63	NPN; type M1163
Q462	48-84411L05	NPN; type M1105
R464L	screened	resistor, fixed: ohms ± 5%; 1/4 W; unless otherwise stated nominal value on schematic
R465 thru 470	screened	nominal values on schematic
R471L	screened	nominal value on schematic
R471M	6-124B57	3.3
R472	screened	nominal value on schematic
R473L	6-11024A37	330; 1/8 W
R473M	screened	nominal value on schematic
R474,475,476	screened	nominal values on schematic
R477L	6-11024A10	24; 1/8 W
R477M	screened	nominal value on schematic
R478L	6-83070E56	2.7
R478M	screened	nominal value on schematic
R479L	screened	nominal value on schematic
R479M	6-11009C25	1k
R480L	screened	nominal value on schematic
R480m	6-124B57	3.3
R481L thru 484L	screened	nominal values on schematic
R485L	6-11041C31	39; 1/8 W
R486L	screened	nominal value on schematic
non-referenced items		
	29-83208M01	LUG, solder; 7-used
	42-83680N03	STRAP, omega; 4-used

**note:** For optimum performance, diodes, transistors, and integrated circuits must be ordered by Motorola part numbers.

# IPA AND 9.6 V REGULATOR (403-435 MHz) SCHEMATIC DIAGRAM



OUTPUT POWER FROM THE IPA VARIES AS A RESULT OF CONTROL VOLTAGE LEVEL APPLIED TO COLLECTORS OF Q460, Q461, AND Q462.

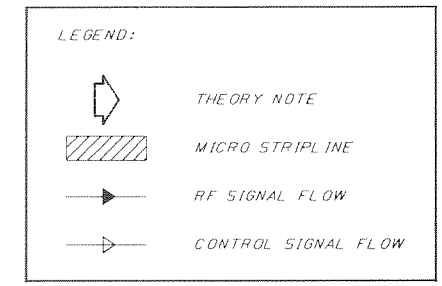
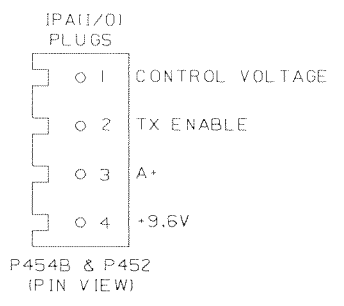
RF OUTPUT TO PA  
0.9 WATTS  
(400-435MHZ)

- NOTES:
- UNLESS STATED OTHERWISE, ALL CAPACITORS ARE IN MICROFARADS AND ALL RESISTORS ARE IN OHMS.
  - ASTERISK (x) INDICATES THICK FILM RESISTOR, NOMINAL VALUE SHOWN.

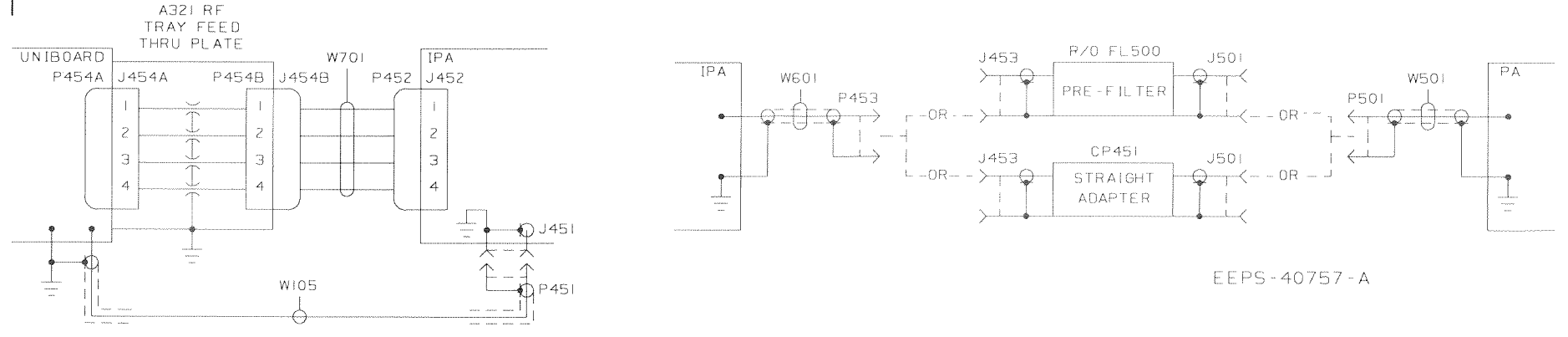
MODEL COMPLEMENT

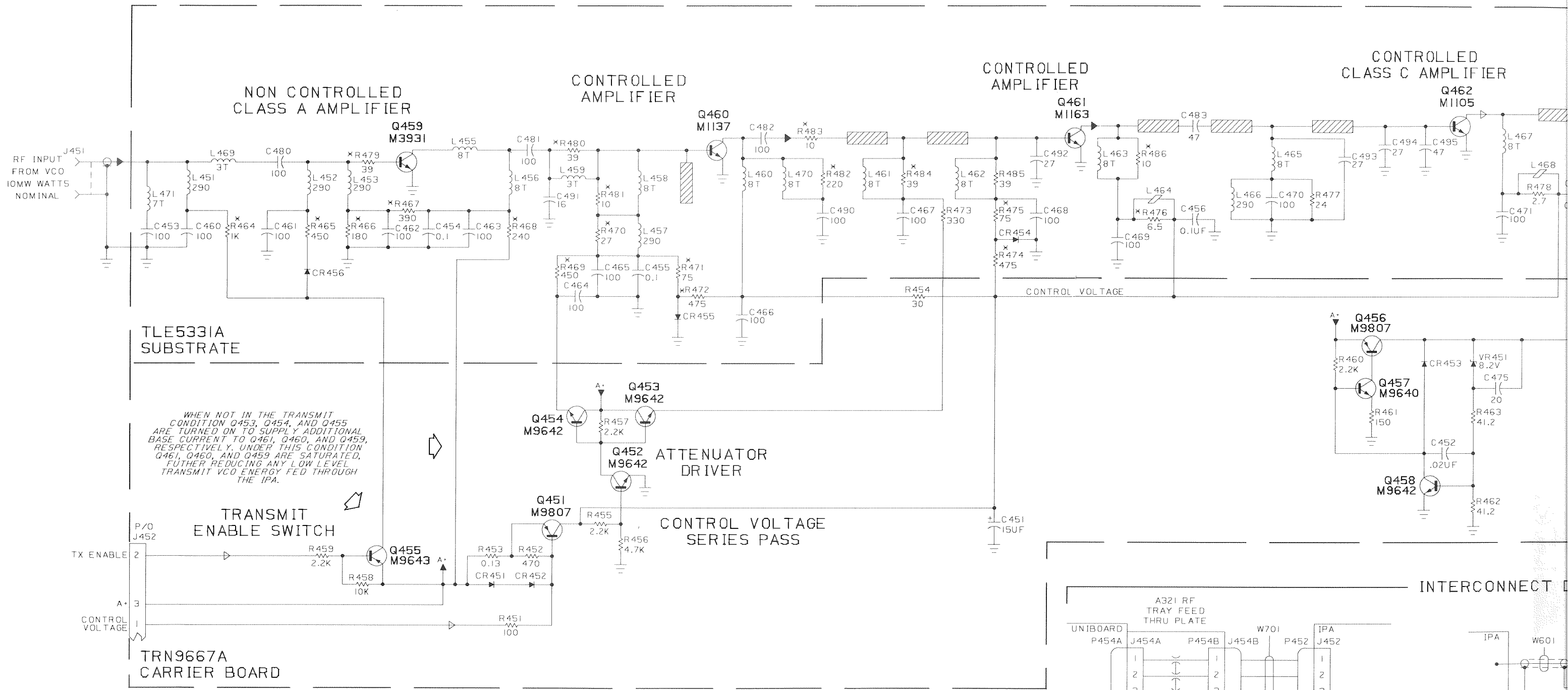
MODEL	DESCRIPTION
TLE5331A	HYBRID CIRCUIT
TRN9667A	CARRIER BOARD
TRN5146A	HARDWARE KIT
TKN8843A	OUTPUT CABLE

### CONNECTOR DETAIL



### INTERCONNECT DETAILS

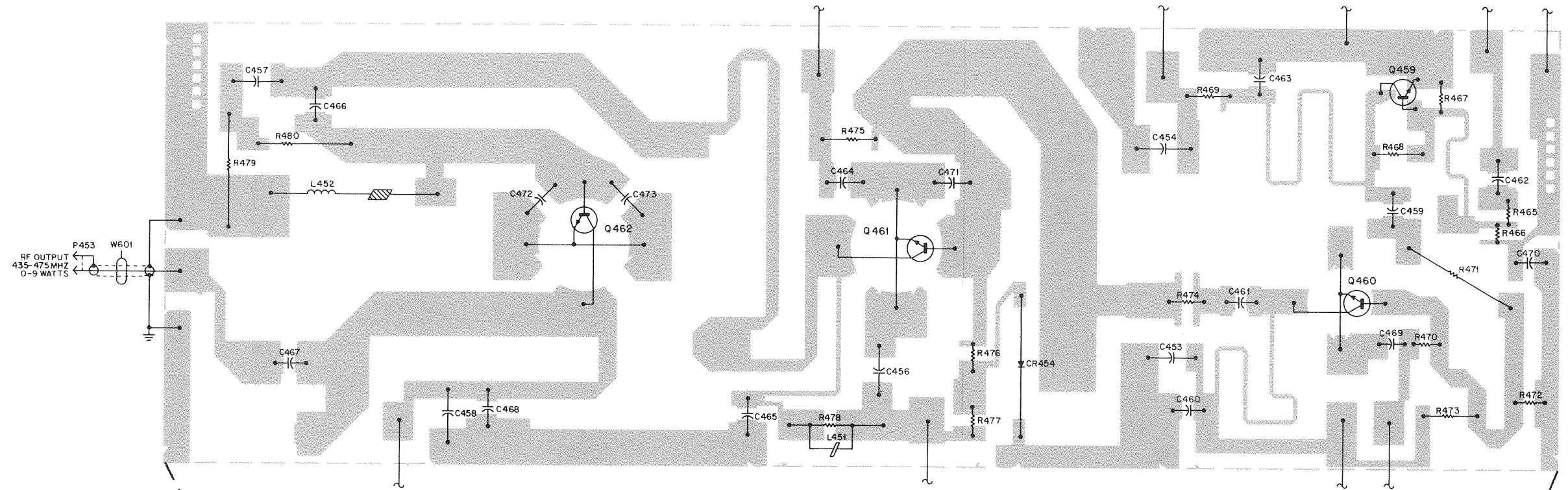




WHEN NOT IN THE TRANSMIT CONDITION Q453, Q454, AND Q455 ARE TURNED ON TO SUPPLY ADDITIONAL BASE CURRENT TO Q461, Q460, AND Q459, RESPECTIVELY. UNDER THIS CONDITION Q461, Q460, AND Q459 ARE SATURATED, FURTHER REDUCING ANY LOW LEVEL TRANSMIT VCO ENERGY FED THROUGH THE IPA.

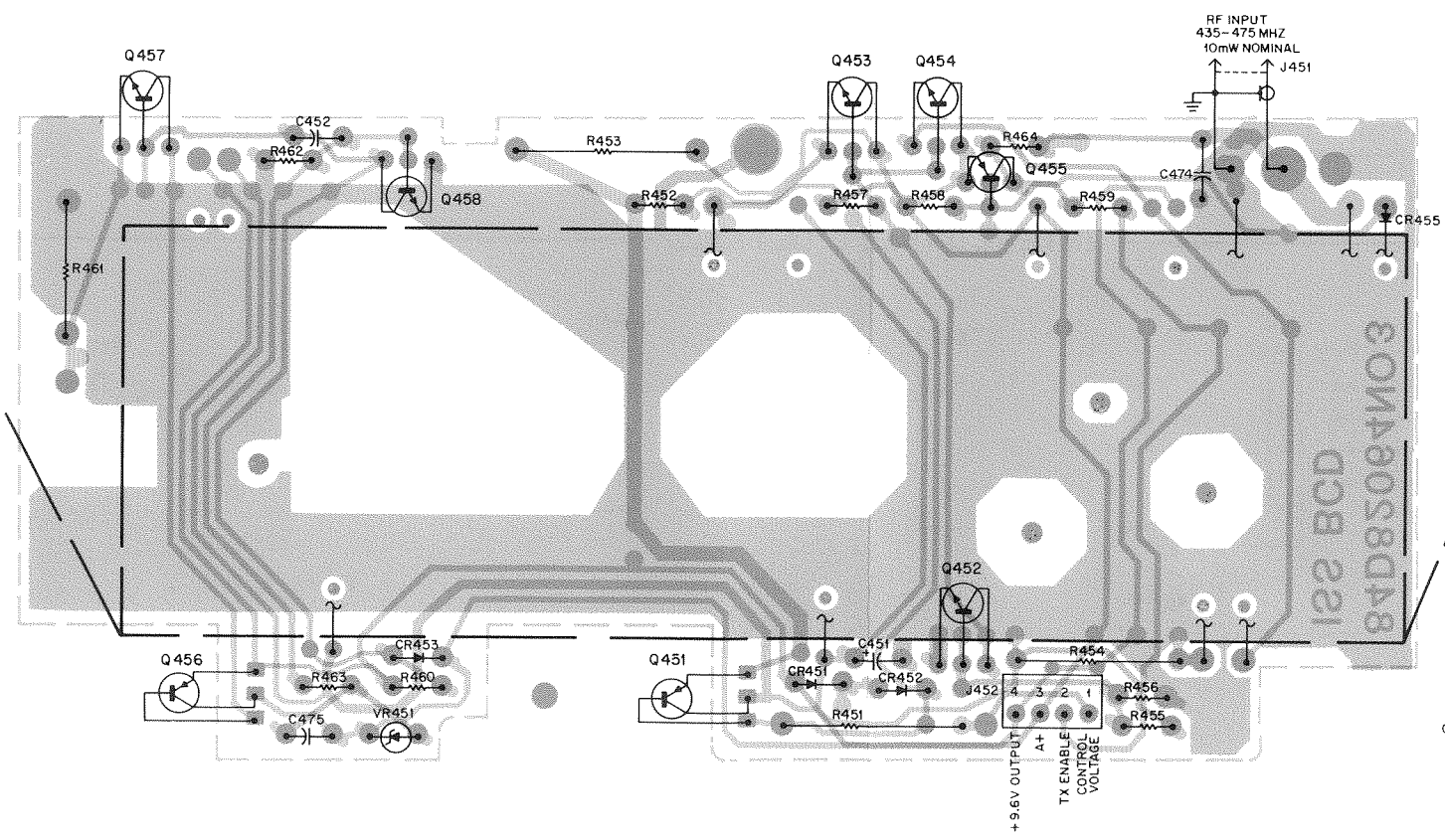
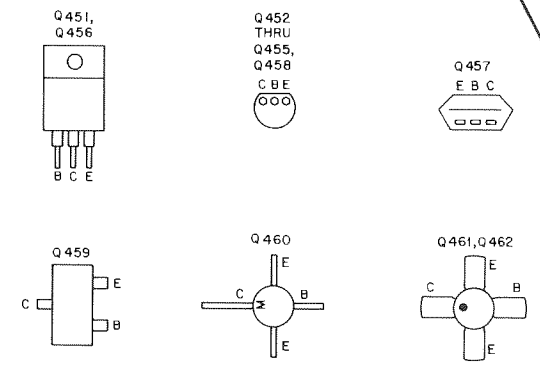
A321 RF TRAY FEED THRU PLATE

**IPA AND 9.6 V  
REGULATOR (435-475 MHz)  
CIRCUIT BOARD DETAILS**



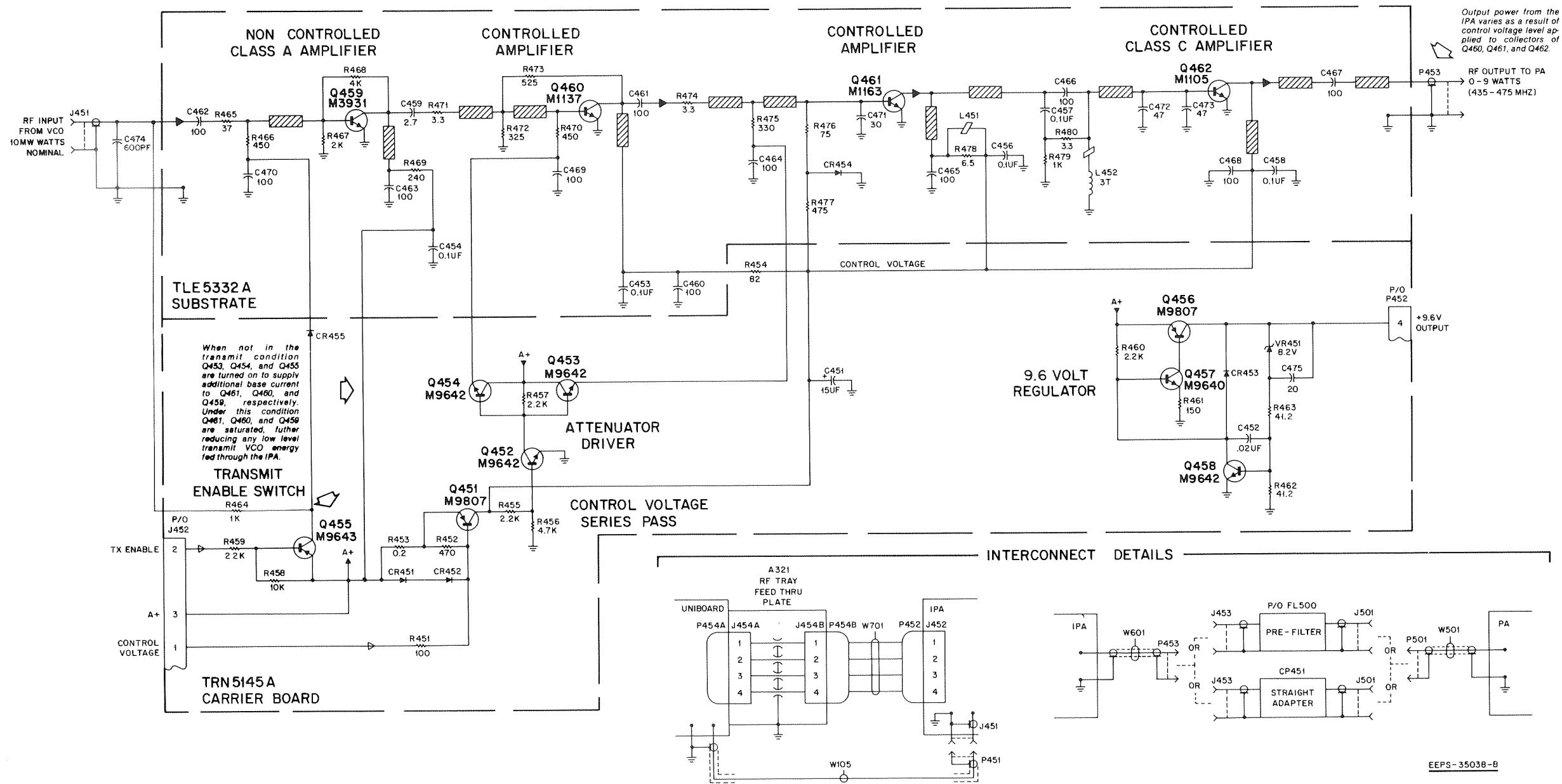
SHOWN FROM COMPONENT SIDE

**TRANSISTOR DETAILS  
TOP VIEWS**



COMPONENT SIDE ● BD-EEPS-37242-0  
SOLDER SIDE ● BD-EEPS-37243-0  
● OL-EEPS-37244-A

# IPA AND 9.6 V REGULATOR (435-475 MHz) SCHEMATIC DIAGRAM



NOTES:

- Unless stated otherwise, all capacitors are listed in picofarads, all resistors in ohms.

Model Complement		
Model	Description	Version
TLE5332A	Hybrid	0
TRN5145A	Carrier Board	0
TRN5146A	Hardware Kit	0





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## 1. GENERAL

The power control circuit can be functionally divided into three main parts:

- RF power leveling
- Power cutback
- Transmitter shutdown

Throughout this discussion, refer to the rf power control loop block and schematic diagrams at the end of this section. In normal operation, power output from the station is controlled by the rf power leveling circuit. This circuit maintains station output power constant over variations in supply voltage and power amplifier temperature. The power cutback circuit reduces station output power under conditions of high temperature, high VSWR, or as directed by station control. If power control is unable to level the power output from the station, a situation exists that is potentially damaging to the station. The transmitter shutdown circuit senses this condition and signals station control to turn off the transmitter.

## 2. RF POWER LEVELING

When a push-to-talk (PTT) signal is generated, the PA KEY line from station control goes low. This turns off Q402 in the power control circuit and enables the IPA for transmission. The low PA KEY signal also causes Q401 to conduct and apply the power set voltage to operational amplifier U402B driving Q403, which produces the control voltage input to the IPA and turns on series pass device Q451. The IPA output drives the power amplifier (PA) and the forward power sensor, located on the PA signal combiner stage senses PA output. The forward power sensor provides a dc signal, FORWARD VOLTAGE, which is proportional to PA output power. The FORWARD VOLTAGE signal is applied to operational amplifier U402B which varies its drive until the FORWARD VOLTAGE is equal to the power set voltage and maintains the two equal. The status of normal power leveling is indicated by the PA ON and PA FULL POWER lines being low and their respective front panel LED's being on.

## 3. POWER CUTBACK

3.1 Station output power is reduced under the following conditions:

1. Station control can generate a power cutback signal by pulling down the PA POWER CUTBACK line. This causes the power set voltage to decrease and reduce station output power. The level of reduction can be varied from 20 percent of rated output to 50 percent of rated output by adjusting R409 in the power control circuit.
2. When the PA heat sink temperature exceeds 100°C, thermistor RT501, (located in the PA), reduces the voltage on the HEAT SINK temperature line. This causes CR403 to conduct and decrease the power set voltage.

3.2 To prevent damage to the PA circulator load when high VSWR's are applied to the station at high ambient temperatures, thermistor RT571 pulls the positive (+) input of comparator U402A below the 3-volt reference on the (—) input, and the output of U402A latches low. In this situation, the station output power is dropped to below 20 percent of the power setting, by the conduction of CR405 pulling down the power set voltage. In the standby mode, Q401 turns off and removes the 3-volt reference from the inverting (—) input of U402A, resetting the comparator.

3.3 Anytime station output power is reduced to 50 percent or less of its set value, the noninverting (+) input of power cutback detector U401B falls below the inverting input, causing its output to go low. This turns off Q404 and signals station control of the reduced power level. Front panel LED, PA FULL, also turns off.

## 4. TRANSMITTER SHUTDOWN

Comparators U401C and U401D detect conditions where power control cannot level the station output power. The output of U401C goes low if the signal on the inverting (—) input of U402B is greater than the power set voltage, indicating station output power is

greater than its set value. If the output of U402B goes to full drive limit (8 volts), the inverting (—) input of U401D rises to 4 volts and the output of U401D goes low. Both comparator outputs are tied together; if either goes low, Q405 turns off and the PA ON signal rises to 3.5 volts, signaling the processor that a control loop failure has occurred. However, when PA ON rises, CR406 stops conducting and the inverting (—) input of comparator U401A rises to 3 volts, latching its output low. This pulls the power set voltage down and reduces station output by 50 percent in an attempt to correct the leveling problem. If the problem is not corrected by this attempt, station control detects that the PA ON signal has remained high and, after 30 msec, removes the PA KEY signal, shutting down the transmitter.

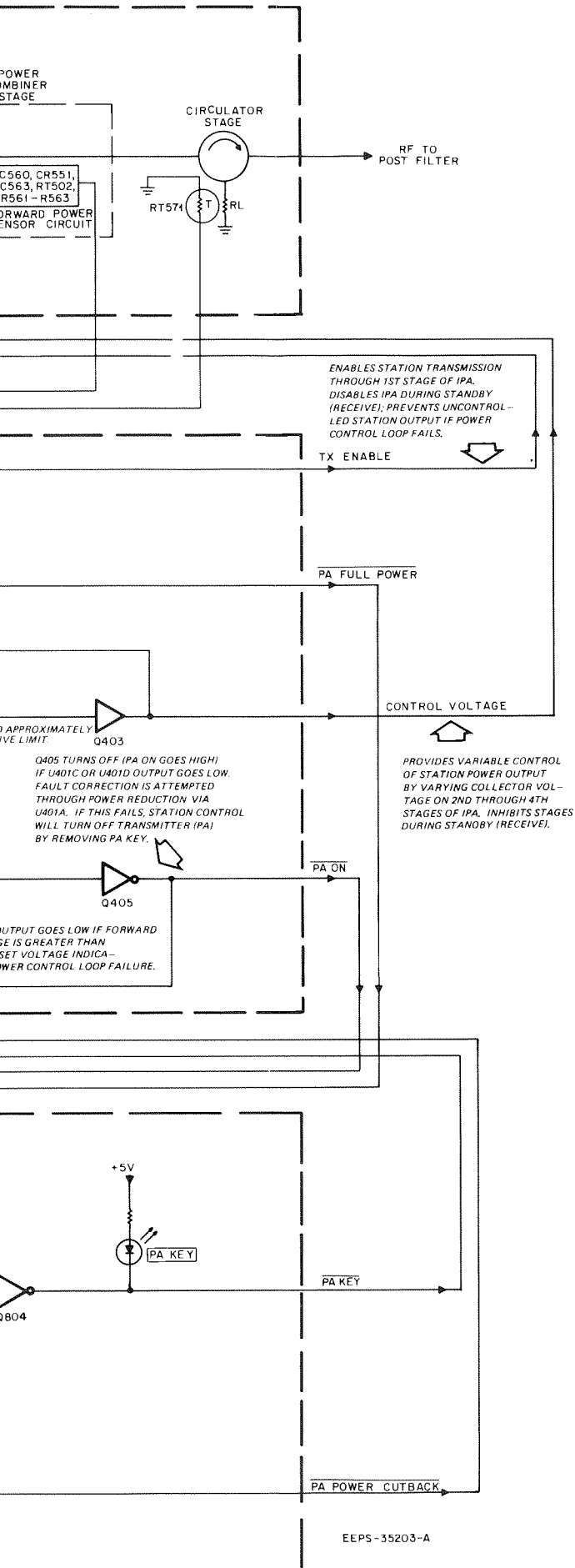
## 5. BATTERY REVERT POWER SET PROCEDURE

Step 1. Set the power output to the rated level by adjusting front panel power set control R426.

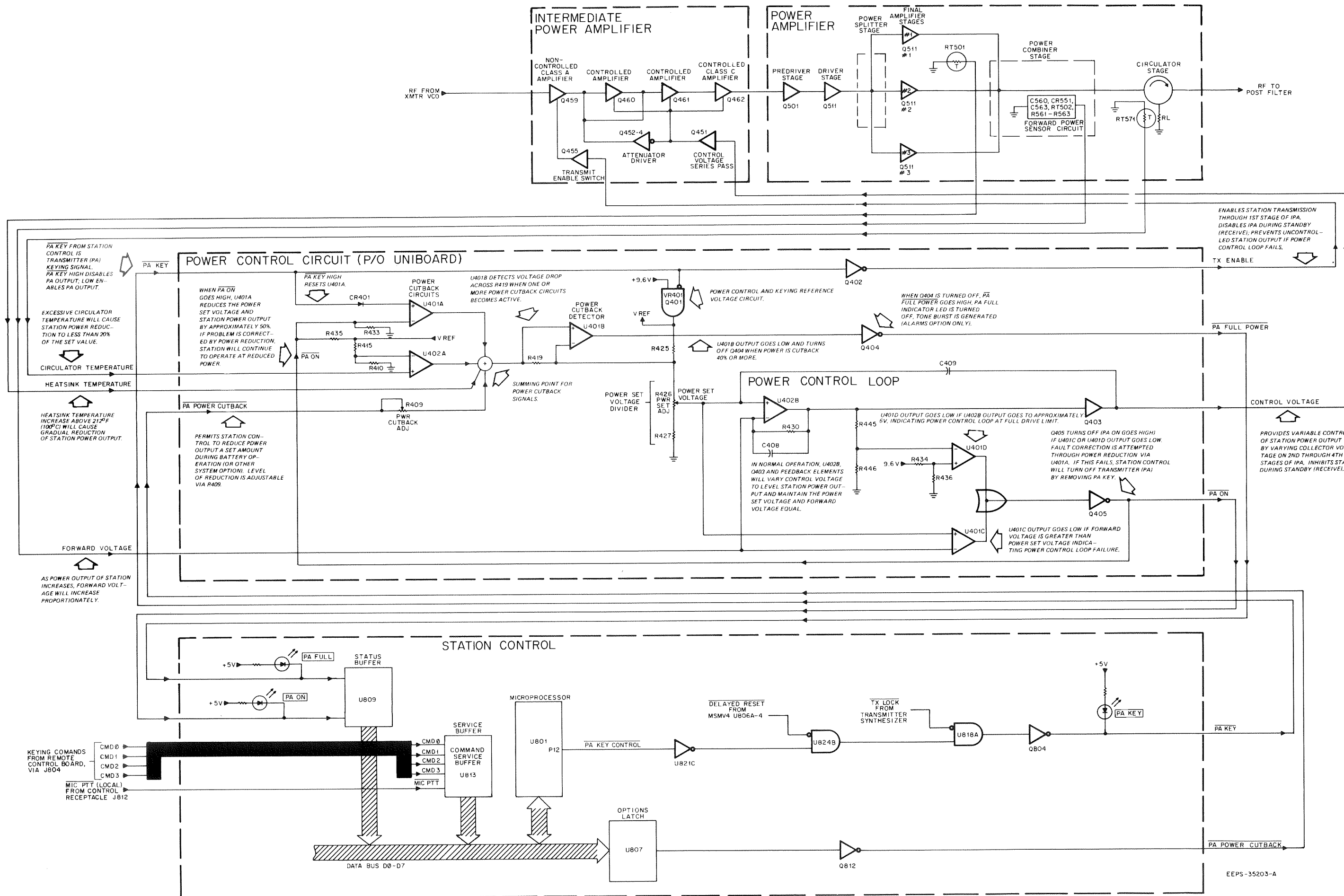
Step 2. With the batteries connected to the station, remove ac power from the station and adjust power cut-back potentiometer R409 for a 50% reduction in power. To access R409, the rf tray cover must be removed to expose the uni-board. R409 is adjustable from the solder side, through the synthesizer shield. (It is not necessary to remove the shield.) Insert tuning tool through shield hole labeled "R409" and adjust.

# POWER CONTROL CIRCUIT

p/o TRN9880A UNIBOARD RF POWER CONTROL LOOP BLOCK DIAGRAM



SEE RF TRAY SECTION FOR  
CIRCUIT BOARD DETAIL AND PARTS LIST



# POWER CONTROL CIRCUIT

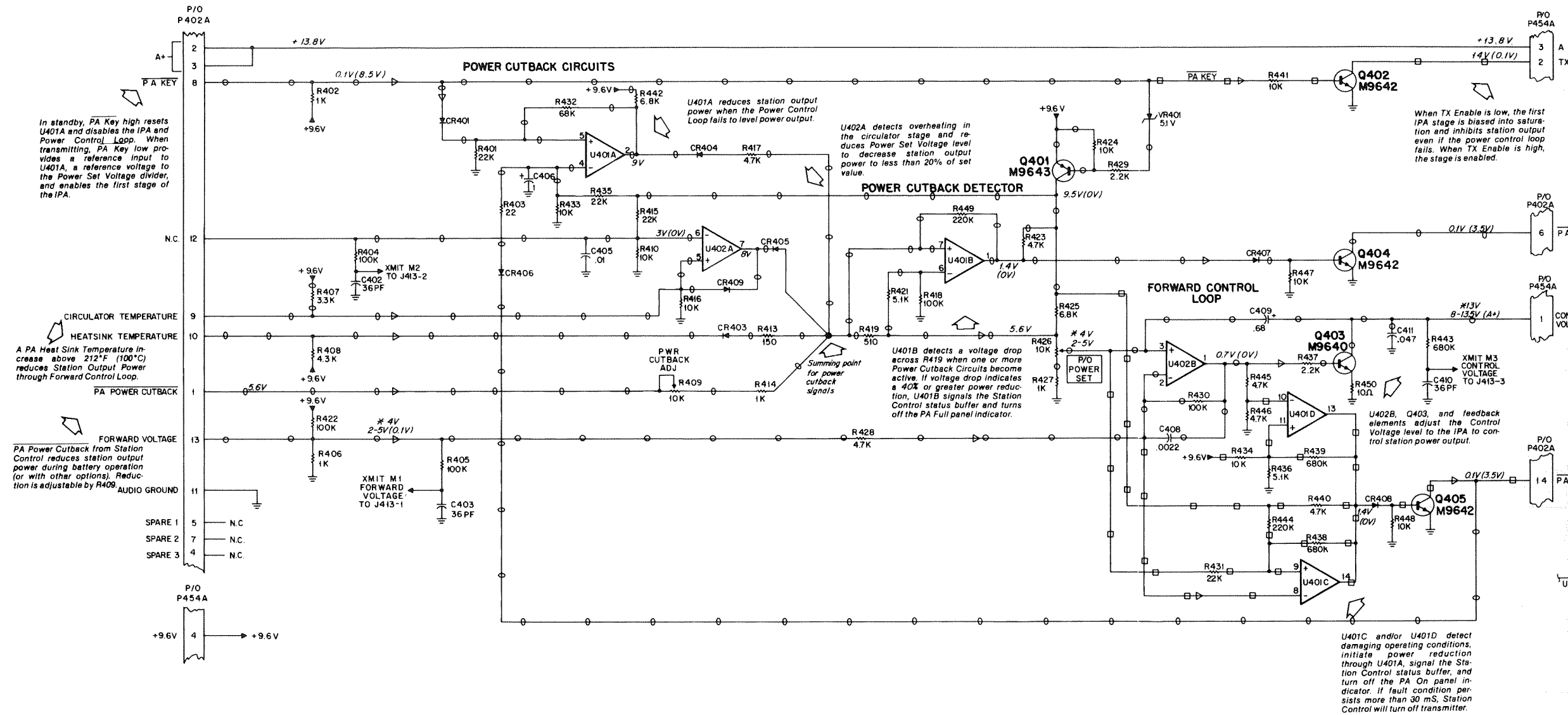
p/o TRN9880A UNIBOARD  
SCHEMATIC DIAGRAM

## NOTES:

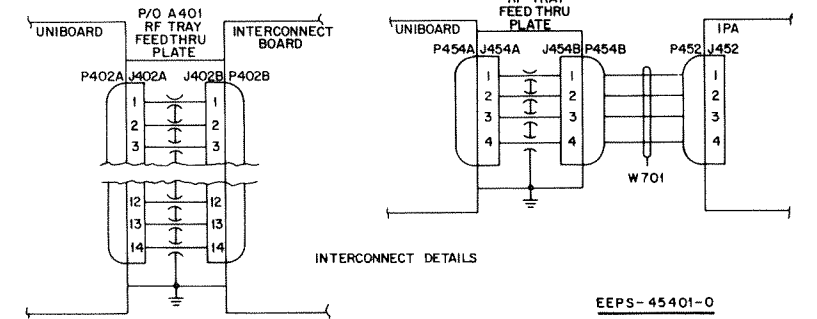
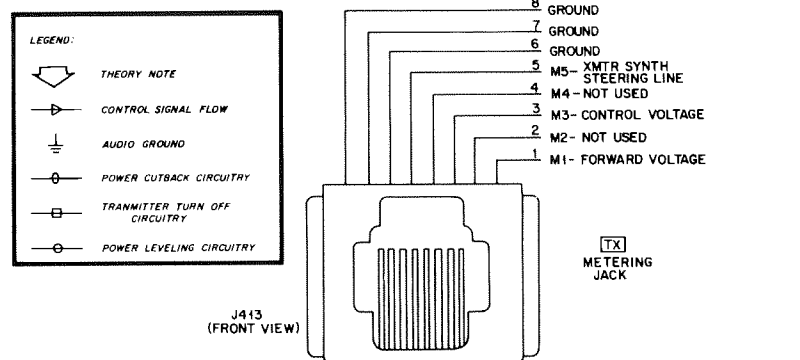
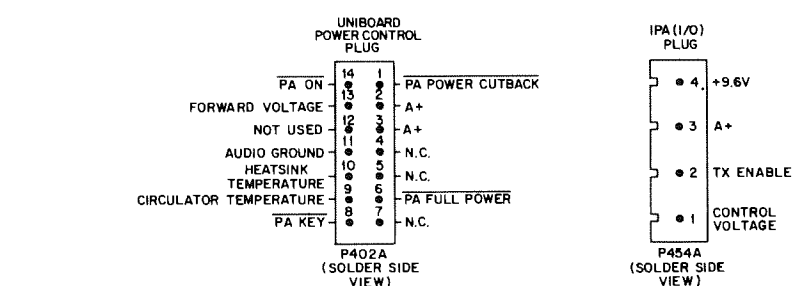
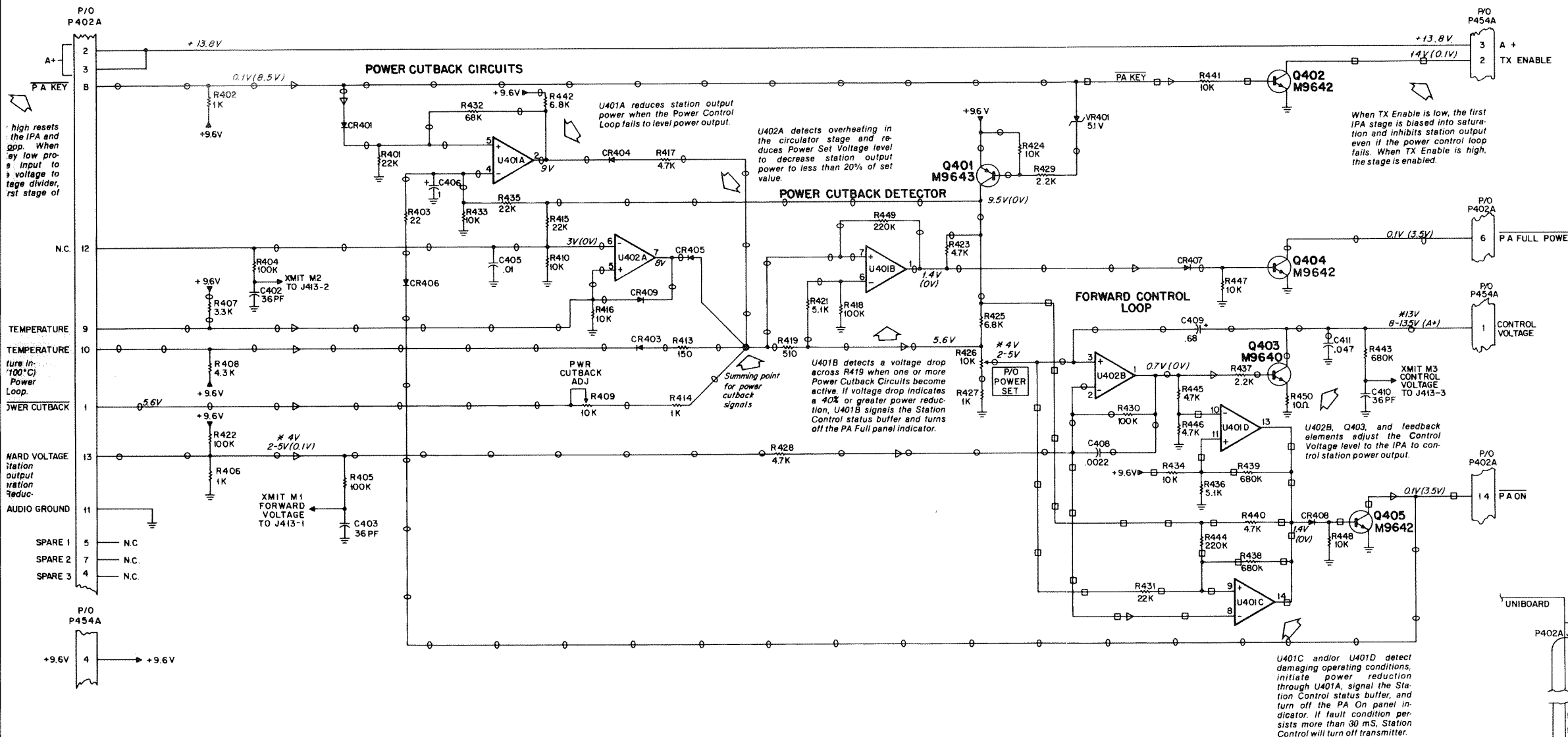
1. Unless otherwise specified, resistor values are in ohms and capacitor values are in microfarads.
2. Voltage references are identified as follows:
  - a. Asterisk (\*) indicates voltage is dependent upon station output level or A— voltage level. Ranges are typical.
  - b. ( ) indicate voltage measured in standby (receive) condition.
  - c. All other voltages measured in transmit condition.
3. Battery charging option may cause control voltage level to decrease 2 to 3 volts in receive condition.

Integrated Circuit Data Chart

Ref. Desig.	-9.5 V (Pin)	Audio Gnd (Pin)	Description
U401	3	12	Quad Comparator
U402	8	4	Dual Op-Amp



SEE RF TRAY SECTION FOR  
CIRCUIT BOARD DETAIL AND PARTS LISTS



U401C and/or U401D detect damaging operating conditions, initiate power reduction through U401A, signal the Station Control status buffer, and turn off the PA On panel indicator. If fault condition persists more than 30 mS, Station Control will turn off transmitter.